

INTRODUCTION: TAP micro-reactors reduce the complexity of industrial operating environments to characterize the catalyst's design. [1] However, the distribution of micron-sized catalyst particles plays a major role in extracting their distinctive reactivity palette and design optimization. [2-4]

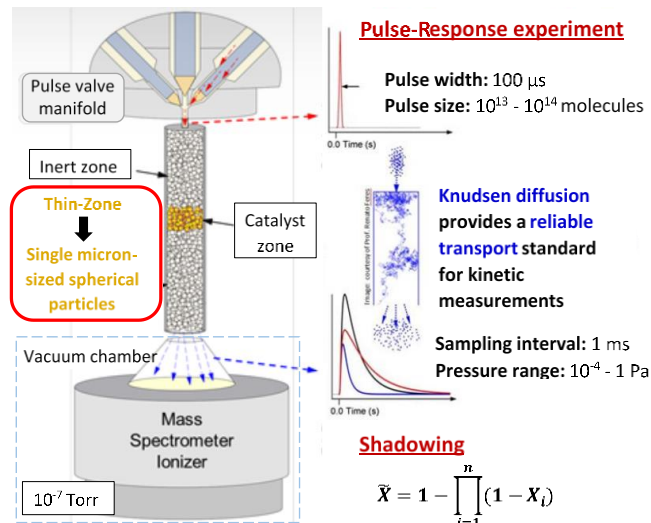


Figure 1. The TAP reactor system: a transient pulse response technique.

RESULTS: Simulations were conducted at 500 K and results were in agreement with the stochastic model.

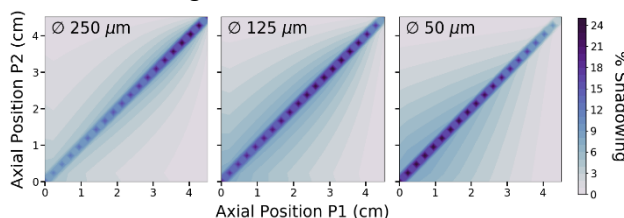


Figure 2. Shadowing of a highly active two-particle system with equal diameter in the axial direction of the TAP reactor.

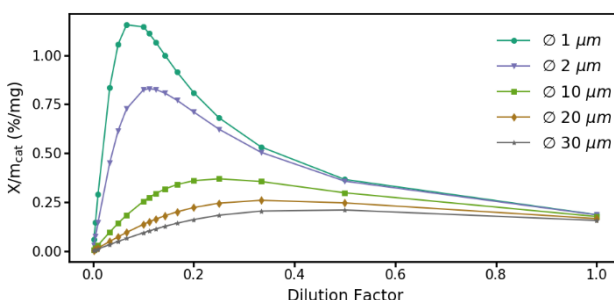


Figure 3. Dilutions of a centered reactive pellet bed of 2 mm long with highly reactive non-porous pellets ($\epsilon_{pe} = 0, D_{pe,i} = 0$).

COMPUTATIONAL METHODS:

Reaction-Diffusion model ($> \phi 50 \mu\text{m}$)

$$\frac{\partial c}{\partial x} \Big|_{x=0} = 1 \rightarrow \frac{\partial c}{\partial t} = D_{cat} \frac{\partial^2 c}{\partial x^2} - kC_G \rightarrow c(t) \Big|_{x=L} = 0$$

Steady-state study in 2- or 3-D Mesh refinement study required

Diluted thin-zone ($\phi 50 - 0.1 \mu\text{m}$)

1-D model with a reactive pellet bed:

$$4\pi N_{pe} \left\{ r^2 r_{pe}^2 \epsilon_{pe} \frac{\partial c_{pe,i}}{\partial t} + \frac{\partial}{\partial r} \left(-r^2 D_{pe,i} \frac{\partial c_{pe,i}}{\partial r} \right) = r^2 r_{pe}^2 R_{pe,i} \right\}, \quad r = \frac{r_{dim}}{r_{pe}}$$

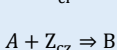
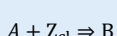
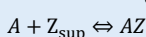
A homogenization approach: $A \rightleftharpoons B$ $R_A = k_f c_A - k_r c_B$

$$k_f = \sqrt{\frac{R_g T}{2\pi M_g}} SSA_{zone} \exp\left(-\frac{E_a^f}{R_g T}\right) \quad R_{A,eff} = R_A SSA_{pellet} r$$

Supported nanoclusters ($\phi 100 - 1 \text{ nm}$)

Inert support (2-D): $\frac{\partial c_s}{\partial t} = \alpha J_{cat} + D_s \Delta c_s - \frac{c_s}{\tau} \rightarrow \sigma_{cz} = \sigma \frac{A_{cz}}{A_{cat}} \left[\frac{\text{mol}}{\text{m}^2} \right]$

TAP reactor: $\frac{\partial c_{AZ}}{\partial t} + \nabla \cdot (D_s \nabla c_{AZ,tangent}) = R_{AZ}$



$$k_f = \frac{P_{stick}}{\sigma_i} \sqrt{\frac{R_g T}{2\pi M_g}} \exp\left(-\frac{E_a^f}{R_g T}\right)$$

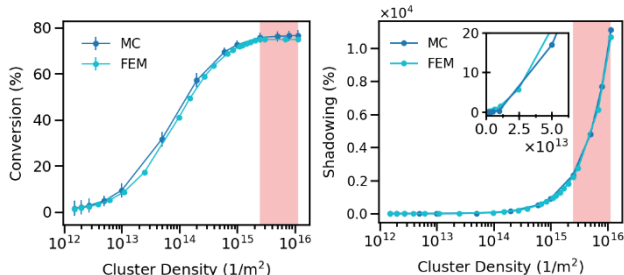
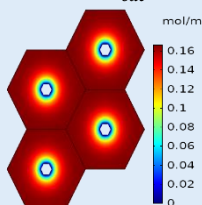


Figure 4. Centered particle (250 μm) deposited with nanoclusters of $\phi 10 \text{ nm}$ at an inert support. Marked red zone = overlap of capture zones.

CONCLUSIONS:

- ❖ Two-Particle system shows most prominent shadowing in the axial direction with a shift towards the inlet of the reactor when decreasing their size.
- ❖ An optimal dilution of a thin-zone can be found at which performance outweighs shadowing.
- ❖ Capture zones extend the distance at which a shadowing effect sets in.
- ❖ Overlap of capture zones stabilizes the conversion, therefore leading to high amounts of shadowing.

A shadowing effect could be simulated for **highly active particles on a multi-scale**. A further step is to extend the models for non-homogeneous catalysts and fine-tune the mode of activity distribution within a catalyst particle with experimental validation.

REFERENCES:

- Zheng, X., Gleaves, J.T., Yablonsky, G.S., Brownscombe, T., Gaffney, A., Clark, M., Han, S. Appl. Catal. A: General 341, 86-92 (2008)
- Gates, B.C. Journal of Catalysis 328, 72-74 (2015)
- Wallace, M., Feres, R., Yablonsky, G., Stern, A. Comput. Chem. Eng. Sci. 125, 612-622 (2019)
- Matolin, V., and Stará, I. Surface Sci. 398, 117-124 (1997)

Deterministic model

Stochastic model

Solution method: Finite elements
Software: COMSOL Multiphysics 5.5

Solution method: Monte Carlo (MC)
In-house software: C++ → Python