

A THERMAL STUDY OF POWER CABLES COOLING IN TUNNELS

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II.EXPERIMENTAL & SIMULATION SETUP

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I – POWER TRANSMISSION NETWORK

From energy production centers to the distribution networks, several solutions are available :



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I – THERMAL LIMITING FACTOR



I – SIMULATION CHALLENGES

□ Tunnels are kilometers long...

→ Long geometries involved

High aspect ratio between the tunnel and the cables

- → High number of elements for a good mesh quality.
- Need of a Low Reynolds approach for high precision in the computed heat transfer.
 - → Even higher number of elements...
- Turbulent flow regime needs a (very) long entrance length.
 - → More elements...









II.EXPERIMENTAL & SIMULATION SETUP

I.Ventilated cable tunnel Mock-up

III.3D numerical simulations

III.CABLE COOLING : RESULTS & DISCUSSION

IV.IMPACT ON THE MAXIMUM PERMISSIBLE CURRENT





II – VENTILATED TUNNEL MOCK-UP





II – COMSOL USE FOR DATA TREATMENT

The experimental data are treated with a coupled MATLAB-COMSOL inverse method.

• The local Nusselt numbers Nu_i are obtained with an optimization script using two parts:

- **The COMSOL heat transfer module** for the heat transfer ¹⁰*W*.*m*⁻².*K*⁻¹ resolution.
 - 2D geometry.
 - Heat conduction in the cables & tunnel walls.
 - Surface-to-surface radiation (hemicube formulation).
 - Heat transfer coefficient at the cable surface controlled by the optimization process in the MATLAB interface.

The mesh is a very fine one

→ Underconstrained model.

Use of an interpolation fonction for the heat transfer coefficient







*h*_{ambient}

Control point for the optimization method



II – COMSOL USE FOR DATA TREATMENT

• The local Nusselt numbers Nu_i are obtained with an optimization script using :

- A MATLAB optimization process based on the minimization of the S criterion (1).
 - A second order regularization is chosen.
 - The regulation coefficient β is optimized for each iterations.

$$S = \sum_{i=1}^{10} (\theta_{comsol} - \theta_{mes})^2 + \beta \sum_{j} (h_{j+1} - 2h_j + h_{j-1})^2 \quad (1)$$

The mean Nusselt number is obtained by integration on the cable surface.

$$\overline{Nu_{D_e}} = \frac{D_e}{2\pi\lambda(\overline{\theta_s} - \theta_{ambient})} \int_0^{2\pi} P_{\text{conv}}(\varphi) \, d\varphi \qquad (2)$$





Cooling profile

Identification process

II – COMSOL USE FOR DATA TREATMENT

The validation case led to a benchmark with the opensource code OpenFOAM and experimental published results.

- □ Similar results obtained.
- OpenFOAM finite volume formulation preferred to COMSOL for the 3D multi-million mesh elements (cluster availability).





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II – 3D NUMERICAL SIMULATIONS

- Simulation RANS using the open source code OpenFOAM.
- Coupled solver and low Reynolds mesh with a turbulence model komega SST.



T fixedValue

Inlet

□ Y+ << 1









II.EXPERIMENTAL & SIMULATION SETUP

III.CABLE COOLING : RESULTS & DISCUSSION

I.Airflow analysis & cable cooling profile II.Mean Nusselt numbers III.New cooling laws

IV.IMPACT ON THE MAXIMUM PERMISSIBLE CURRENT



III – AIRFLOW ANALYSIS & CABLE COOLING PROFILE

□ As the cable wall spacing decreases, the air flow structure deforms itself.

□ A velocity drop is observed in the gap between cable and wall.





III – AIRFLOW ANALYSIS & CABLE COOLING PROFILE

- The observed velocity drop can be down to 50% of the entrance velocity.
- A threshold wall spacing value of Lx = 2De can be defined.





III – MEAN NUSSELT NUMBERS

- The depreciation of mean Nusselt number is clearly obtained, with a 20% drop for very close proximity with a wall (Lx = 0.5De).
- □ Heat transfer 2 times less important as regards to the current cooling law [1].

Possible reasons :

- Turbulence entrance length not reached in [1].
- Studies without support elements (brackets).

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IV – IMPACT ON THE MAXIMUM PERMISSIBLE CURRENT

Using the design tool for underground power cables with the new laws, the impact on the maximum transmissible current in the power link can be tested.

Idealized case (no brackets, no corkscrewing effects, etc.)



L = 1 km

Max. operating temperature: 90°C in the core

	Weedy and El Zayyat	$Nu_{De}(Lx/De)$	Weedy and El Zayyat I = 2354 A	
T core (°C)	89,96	89,97	79,16	- 1
T air (°C)	30,41	28,86	28,8	
h wall (W/m².K)	2,91	2,91	2,91	
h cable (W/m².K)	9,35	3,96	9,37	
l max (A)	2526	2354	2354	







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V - CONCLUSION

- Experimental & numerical studies have highlighted the impacts of the proximity to a tunnel wall and the flow development.
 - □ The depreciation of the heat transfer can be of 20% for close installations to a wall.

On-going work.

- □ Cable groups effects on the heat transfer (two cables and trefoil configurations).
- Effects of the support elements.

Wish list

- \Box Get rid of the OpenFOAM platform for the 3D \rightarrow have COMSOL simulate everything.
- A mean to simulate details local heat transfer for very long geometries with limited mesh elements (ideas ?).
- □ Or else, a full COMSOL cluster license...









THANK YOU

ANY QUESTIONS



