

Topology Optimization of Thermal Heat Sinks

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Outline of presentation

- Introduction to topology optimization
- Thermofluid model
 - Heat sink topology optimization model
 - Fluid dynamics modeling
 - Heat transfer modeling
- Results
 - Optimized designs
 - Parameter studies
- Summary and outlook

Topology optimization – introduction

- What is topology optimization?
 - Originated in structural mechanics
 - Optimal material distribution in given design domain
- Density-based topology optimization
 - Design variable field $\gamma: 0 \rightarrow \text{solid}; 1 \rightarrow \text{void}$
 - Problem relaxed to γ values between 0 and 1 $\rightarrow Gradient\mbox{-based}$ optimization possible
- Advantages of topology optimization
 - Systematic design approach
 - Can yield unintuitive structures



Shape variables



Thermofluid topology optimization model

- Forced convection cooled heat sink
- Possible applications
 - CPU cooling
 - Thermoelectric generators
- Optimization objective
 - Minimization of solid plate temperature for prescribed pressure drop
- Topology optimization carried out with Optimization Module and LiveLink for MATLAB
 - Optimization method: MMA



Fluid dynamics modeling

- Implemented in CFD Module
- Assumptions
 - Stationary laminar flow
 - Incompressible fluid
 - 2D
- Incompressible Navier-Stokes and continuity equation

$$\rho_{fl} \cdot (\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla p + \mu (\nabla^2 \mathbf{u}) - \alpha(\gamma) \mathbf{u} \qquad \nabla \cdot \mathbf{u} = 0$$

- Interpolation of artificial friction force
 - Fluid region $\gamma = 1 \Rightarrow \alpha = 0 \Rightarrow NS \ equation$
 - Solid region $\gamma = 0 \Longrightarrow \alpha = \alpha_{\max} \approx \infty \Longrightarrow \mathbf{u} = \mathbf{0}$





Heat transfer modeling

- Implemented in Heat Transfer Module
- Heat transfer in fluid outside design domain
- Heat transfer modeling in design domain
- Heat transfer in solid plate
- Interpolation of
 - Thermal conductivity in design space
 - Out of plane heat transfer between solid and fluid layer



$$\rho_{fl}c_{fl}\mathbf{u}\cdot\nabla T_{fl} - \nabla\cdot(k_{fl}\nabla T_{fl}) = 0$$

$$\rho_{fl}c_{fl}\mathbf{u}\cdot\nabla T_{fl} - \nabla\cdot(k(\gamma)\nabla T_{fl}) = \frac{h(\gamma)(T_s - T_{fl})}{dz_{fl}}$$

 $\nabla (1 \nabla T)$

Λ

$$-\nabla \cdot (k_s \nabla T_s) = \frac{q_{prod}}{dz_s} - \frac{h(\gamma)(T_s - T_{fl})}{dz_s}$$





Results optimization



Results – effect of pressure drop



- \rightarrow More and bigger fins with increasing Δp
- \rightarrow Bumps on fins increase with increasing Δp



Parameter studies – optimized structures



→Decreasing plate temperature with increasing Δp →Generally Re increases with increasing Δp →Re can decrease with Δp if new fin is added to design

Summary and Outlook



<u>Summary</u>

- Thermofluid topology optimization model implemented in COMSOL Multiphysics
- Optimized designs and parameter studies presented

→ COMSOL Multiphysics allows for relatively straightforward implementation of topology optimization

<u>Outlook</u>

- Validation of 2D topology optimization
 - Full 3D optimization
 - Experimental comparison to standard structures

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Backup

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Thermofluid heat sink model II

Boundary conditions thermofluid design layer





COMSOL for topology optimization

- Advantages
 - Straightforward multiphysics modeling
 - MMA optimizer implemented
 - PDE filter can be easily added
 - Advanced post-processing tools available
- Drawback
 - Limited scalability for large scale optimization



Topology optimization – filter and projection

- Density filter needed to provide regularization for the optimization problem
- Implemented as PDE filter within COMSOL's "Coefficient Form PDE interface"

$$-r^2\Delta\widetilde{\gamma}+\widetilde{\gamma}=\gamma$$

- Three-field topology optimization
 - Design variable: γ
 - Density filter (PDE) $\rightarrow \tilde{\gamma}$
 - Smoothed Heaviside projection $\rightarrow \bar{\tilde{\gamma}}$







Heat transfer modeling - complete

- Heat transfer modeling solid plate
- Heat transfer modeling fluid
- Heat transfer modeling design space

- Interpolation of
 - Out of plane heat transfer between solid and fluid layer
 - Thermal conduction in design space

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$$-\nabla \cdot (k_s \nabla T_s) = \frac{q_{prod}}{dz_s} - \frac{h(\gamma)(T_s - T_{fl})}{dz_s}$$



$$\rho_{fl}c_{p,fl}\mathbf{u}\cdot\nabla T+\nabla\cdot(-k(\gamma)\nabla T)=\frac{h(\gamma)\cdot(T_s-T_{fl})}{dz_s}$$

$$h(\gamma) = h_{\min} \frac{\gamma(C_h(1+b_h)-1)+1}{C_h(1+b_h\cdot\gamma)}$$

$$k(\gamma) = k_{fl} \frac{\gamma(C_k(1+b_k)-1)+1}{C_k(1+b_k\cdot\gamma)}$$

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Mesh – Fluid-thermal layer



References

Bendsøe et al. 2003 → TopOpt Buch

Navier-Stokes equations

Incompressible Navier-Stokes equation for porous flow

$$\mathbf{u} \cdot \nabla \mathbf{u} - \frac{1}{Re} \nabla \cdot (\nabla \mathbf{u}) + \boldsymbol{\alpha} \mathbf{u} + \nabla p = \mathbf{0}$$
$$\nabla \cdot \mathbf{u} = \mathbf{0}$$
Non-fluid (solid) region

 $\rho = 0 \Rightarrow \alpha = \overline{\alpha} \approx \infty \Rightarrow u = 0$

Fluid region

 $\rho = 1 \Rightarrow \alpha = 0 \Rightarrow NS$ equation

Interpolation scheme

$$\boldsymbol{\alpha}(\rho) = \bar{\alpha} \frac{1-\rho}{1+q_{\alpha}\rho}$$

Incompressible Navier-Stokes equation for porous flow

$$\mathbf{u} \cdot \nabla \mathbf{u} - \frac{1}{Re} \nabla \cdot (\nabla \mathbf{u}) + \boldsymbol{\alpha} \mathbf{u} + \nabla p = \mathbf{0}$$

 $\nabla \cdot \mathbf{u} = 0$

Convection-diffusion equation

$$\mathbf{u} \cdot \nabla T - \nabla \cdot (\mathbf{K} \nabla T) = \mathbf{0}$$