

Thermomechanical modeling of dislocation density increase during PVT growth of SiC crystals

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COMSOL
CONFERENCE
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Outline

- Context and motivation : Physical Vapor Transport and dislocations
- Alexander-Haasen model & COMSOL implementation
- Cooling of a mono-crystal and increase of dislocation density
- Prospects : crystal growth and 3D modeling
- Conclusion

Physical Vapor Transport growth of single SiC crystals

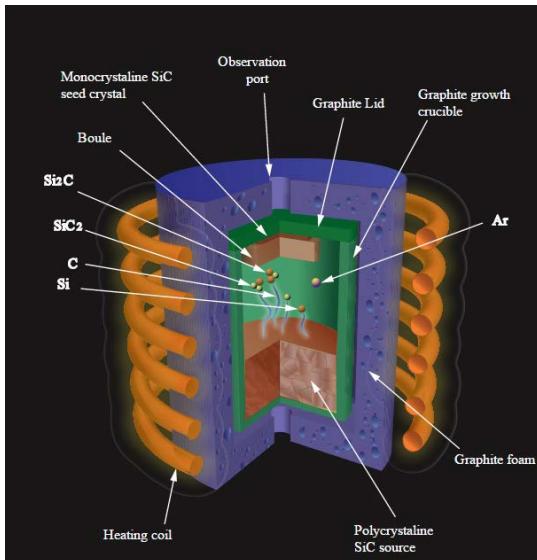
Induction heating

Very high temperatures ($2300\text{ }^{\circ}\text{C}$)

Applications : abrasives,
wafers for power electronic
devices ...



(Wikipedia)



(Wikipedia)



LMGP PVT reactor

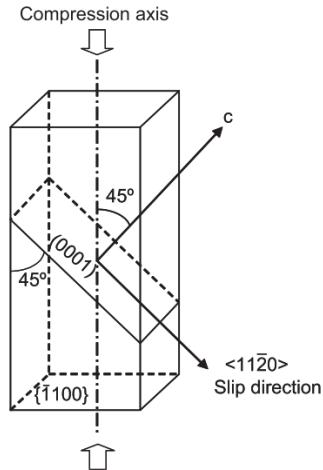
Thermal
gradients

Thermal
stresses

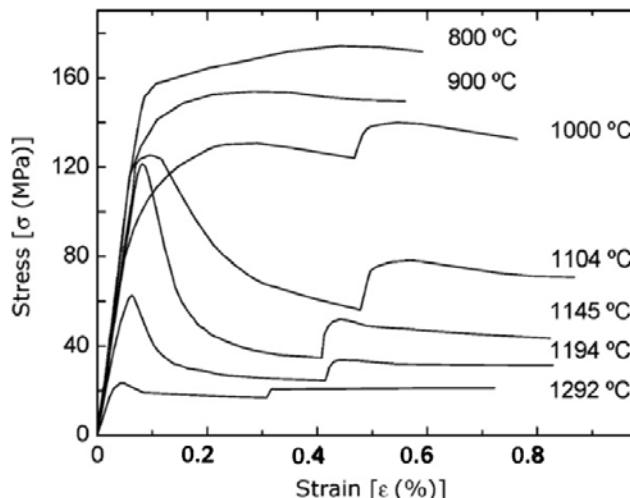
Plasticity
($T=2300\text{ }^{\circ}\text{C} !$)

Dislocation
density increase

- Mechanical behavior of SiC at very high temperature



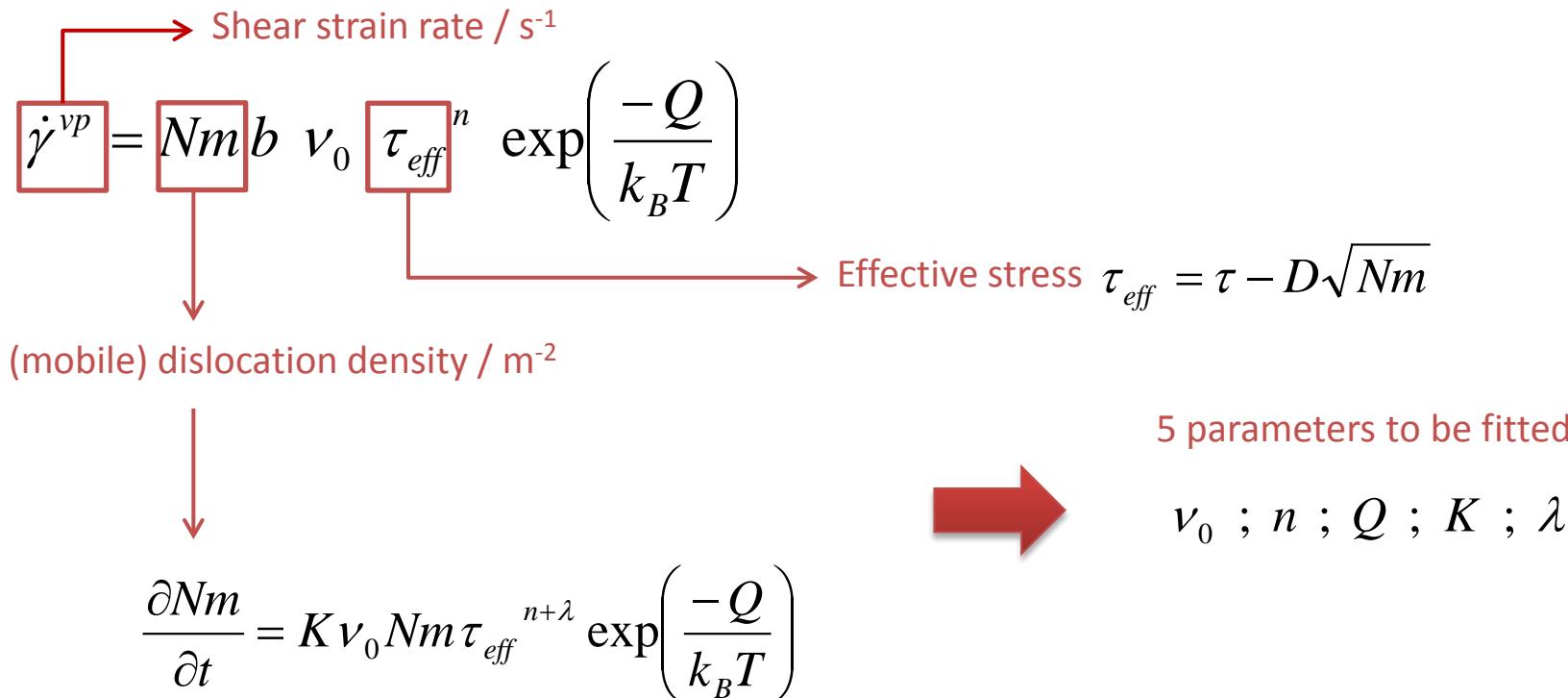
Single hcp crystal
Dislocations glide along
basal plane (0001)



Highly anisotropic
viscoplasticity

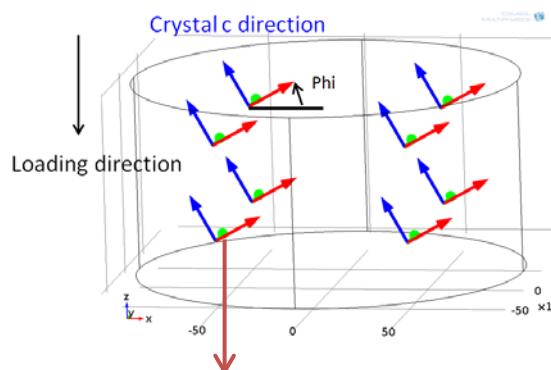
Lara et al., *Ceram. Int.* **38**, 1381–1390 (2012).

- Alexander-Haasen model : viscoplasticity with internal variable

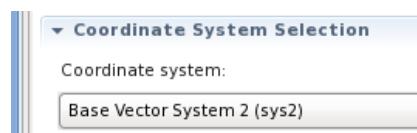


● Alexander-Haasen model : COMSOL implementation

Calibration compression test (3D)



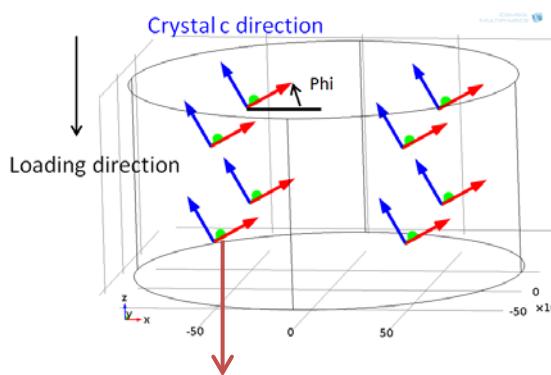
Coordinate system associated with behavior law



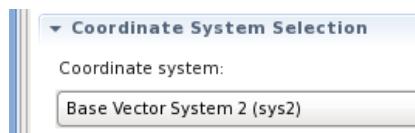
NB : nonlinear structural materials module is required

Alexander-Haasen model : COMSOL implementation

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Coordinate system associated with behavior law



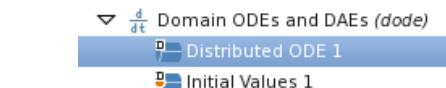
Domain ODE governing dislocation density rate

Equation

Show equation assuming:
Study 1, Time Dependent

$$\epsilon_a \frac{\partial^2 Nm}{\partial t^2} + d_a \frac{\partial Nm}{\partial t} = f$$

Source Term

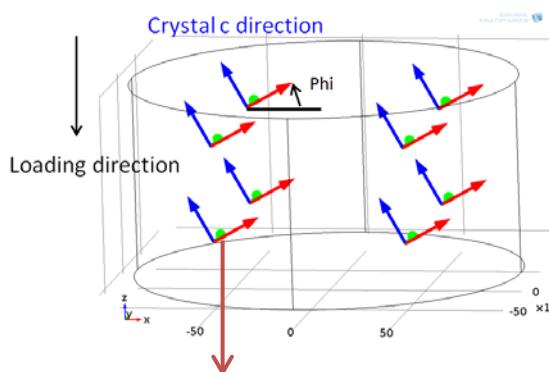
$$f = K \nu_0 Nm \tau_{eff}^{n+\lambda} \exp\left(\frac{-Q}{k_B T}\right)$$


$$\frac{\partial Nm}{\partial t} = K \nu_0 Nm \tau_{eff}^{n+\lambda} \exp\left(\frac{-Q}{k_B T}\right)$$

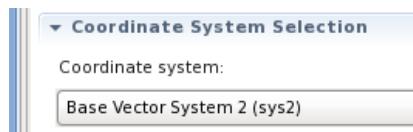
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Alexander-Haasen model : COMSOL implementation

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Domain ODE governing dislocation density rate

Equation

Show equation assuming:
Study 1, Time Dependent

$$\epsilon_a \frac{\partial^2 Nm}{\partial t^2} + d_a \frac{\partial Nm}{\partial t} = f$$

Source Term

$$f = [K * \nu_0 * Nm * \tau_{eff}^{n+\lambda} * \exp(-Q / (k_B T))] / m^2$$

Domain ODEs and DAEs (dode)

- Distributed ODE 1
- Initial Values 1

$$\frac{\partial Nm}{\partial t} = K \nu_0 Nm \tau_{eff}^{n+\lambda} \exp\left(\frac{-Q}{k_B T}\right)$$

Anisotropic elasticity + creep strain rate

Creep Data

Material model:
User defined

Creep rate tensor:

0	0	0.5*Nm*b*nus
0	0	0
0.5*Nm*b*nus	0	0

F_{cr} 1/s

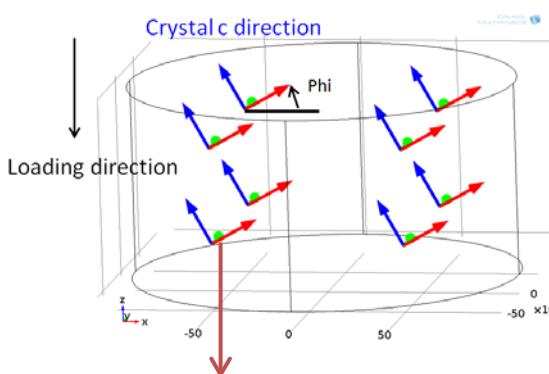
Solid Mechanics (solid)

- Linear Elastic Material 1
- Creep 1

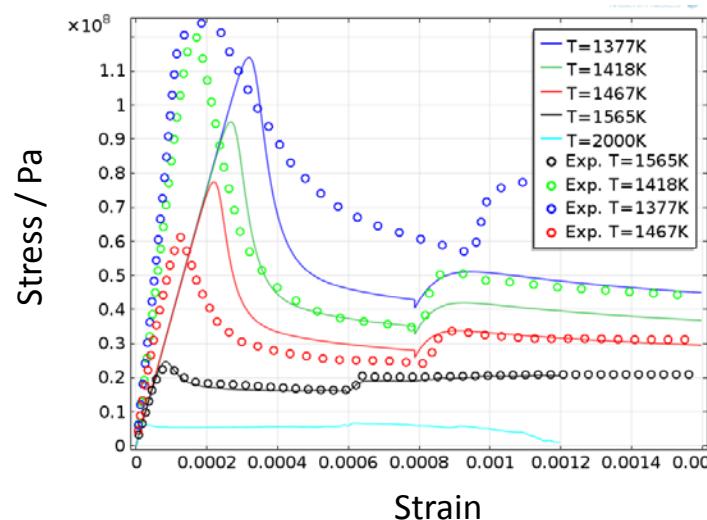
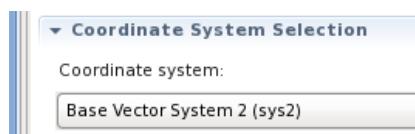
$$\dot{\gamma}^{vp} = Nm b \nu_0 \tau_{eff}^n \exp\left(\frac{-Q}{k_B T}\right)$$

● Alexander-Haasen model : calibration / validation

Calibration compression test (3D)



Coordinate system associated with behavior law



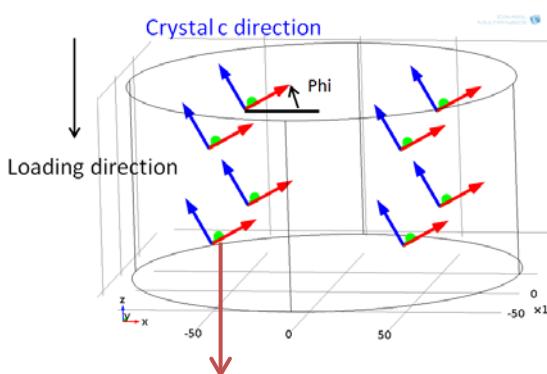
$$\nu_0 = 8.5E-15; n = 2.8; Q = 3.3eV; K = 7E-5; \lambda = 1.1$$

Gao et al., *Cryst. Growth Des.*, **14**, 1272-1278 (2014)

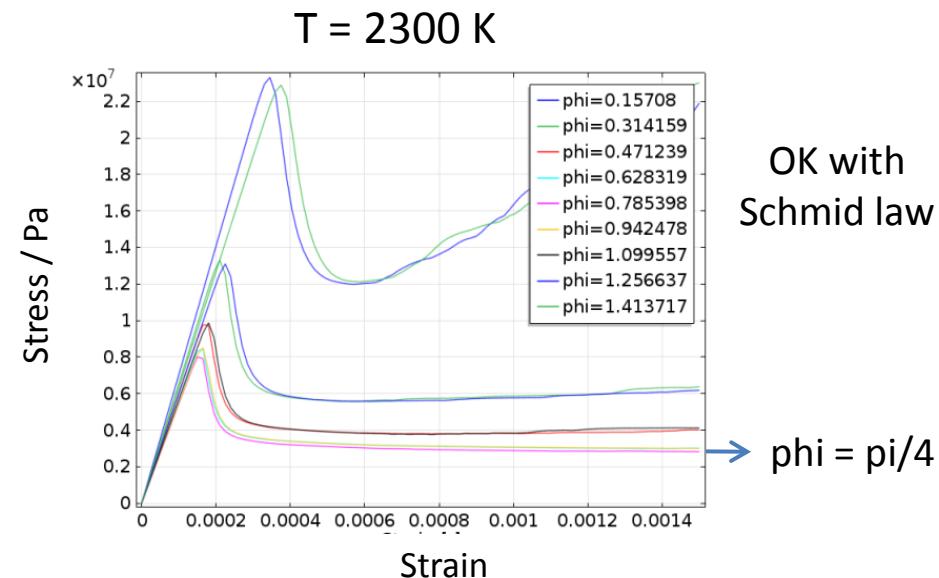
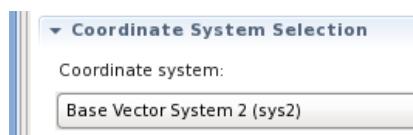
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● Alexander-Haasen model : calibration / validation

Calibration compression test (3D)



Coordinate system associated with behavior law

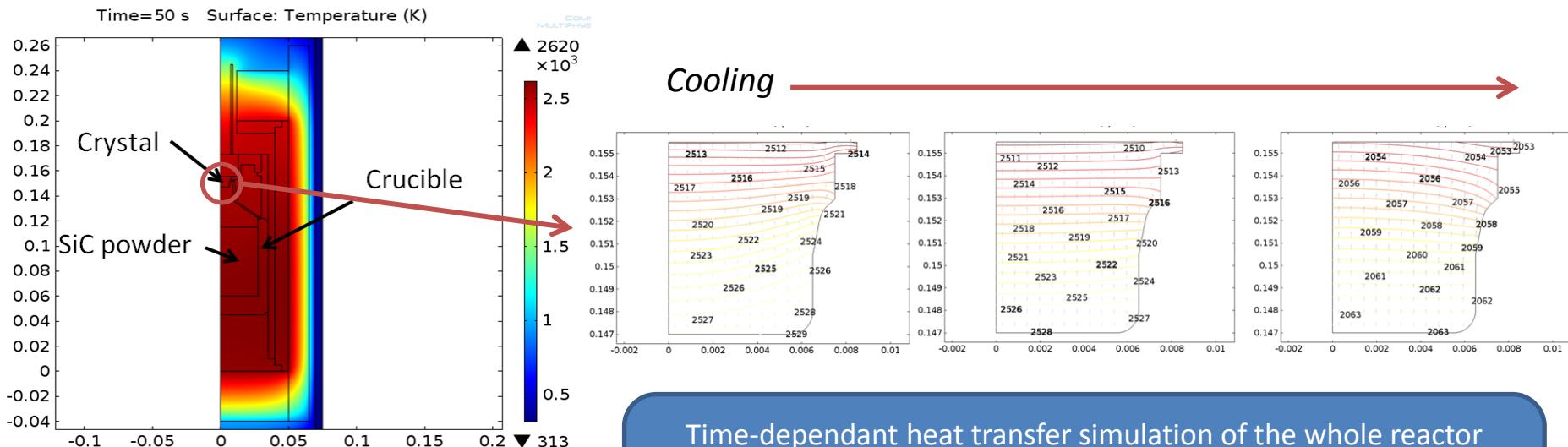


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NB : nonlinear structural materials module is required

- Crystal shape and thermal field from thermo-chemical simulation^[1]



Time-dependant heat transfer simulation of the whole reactor

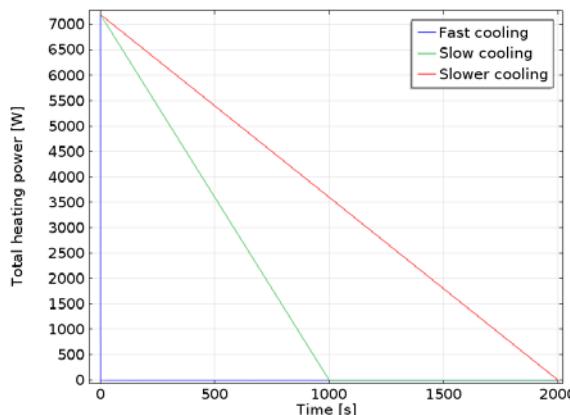
+

Time-dependant mechanical simulation of thermal stresses with
temperature dependant behavior for the crystal

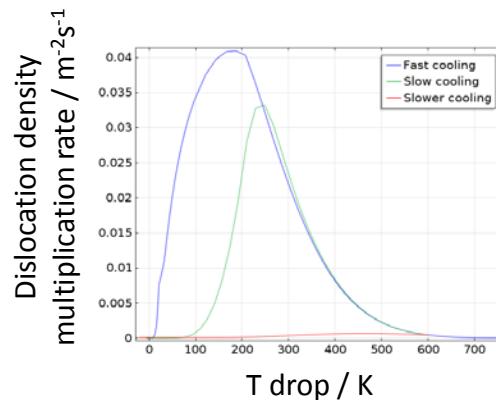
[1] Ariyawong, K. et al., *Materials Science Forum*, **778-780**, 35-38 (2014).

Effect cooling velocity

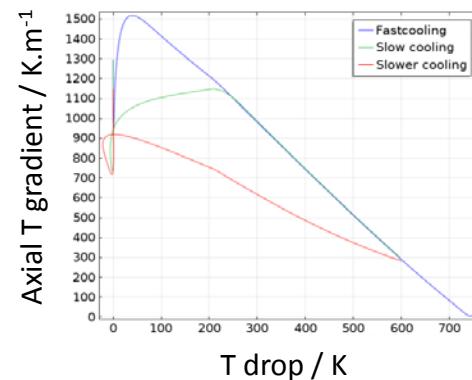
Cooling profiles



Induction heating = internal heat source



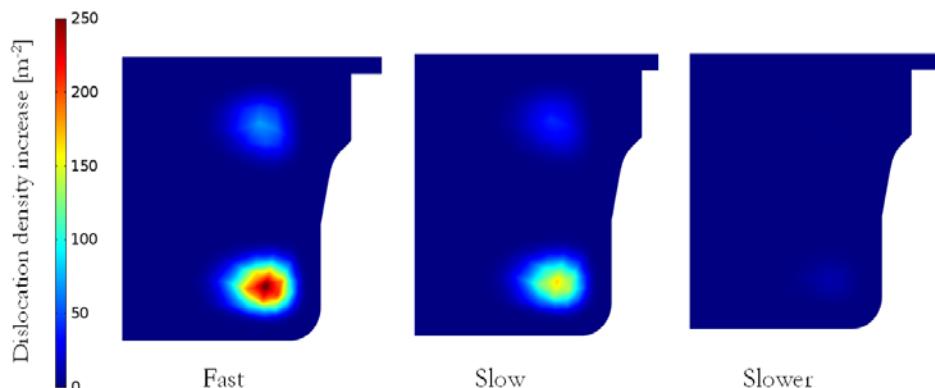
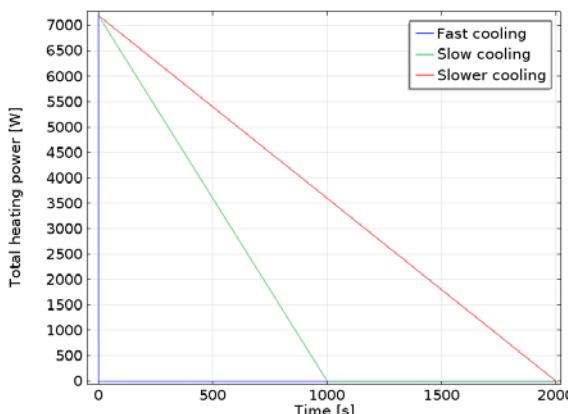
Dislocation density increase very low under 1800K



Slow cooling minimize axial temperature gradient

Effect cooling velocity

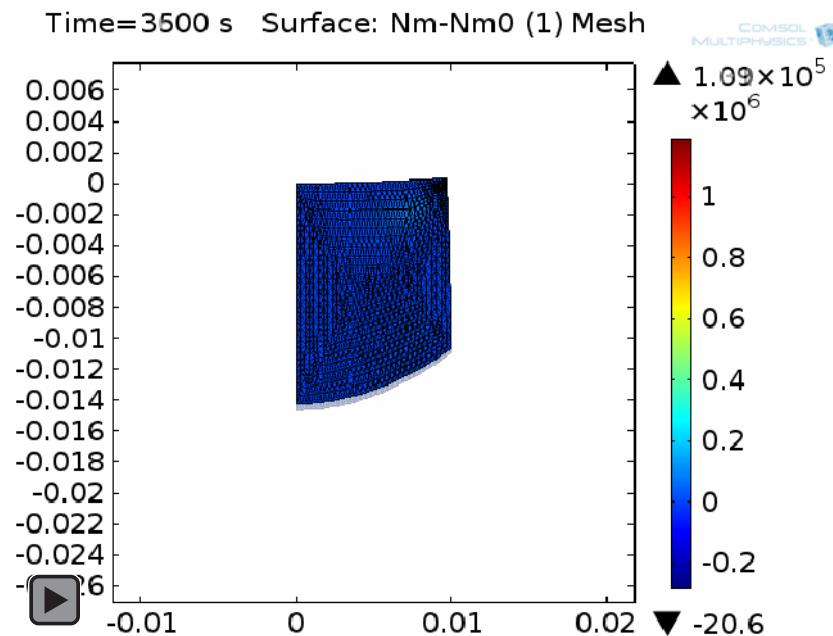
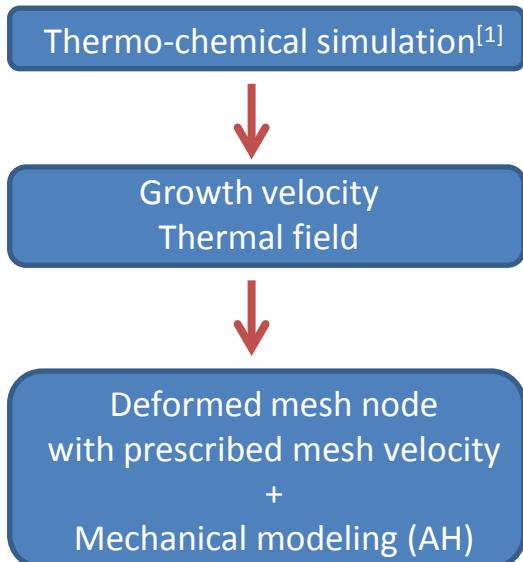
Cooling profiles



*Induction heating = internal
heat source*

- Prospects : dynamic crystal growth simulation

Motivation : dislocations actually mainly develop during growth !



[1] Ariyawong, K. et al., *Materials Science Forum*, **778-780**, 35-38 (2014).

● Prospects : 3D modeling

Motivation : off-axis orientation of the crystal

2D axisymmetric heat transfer
simulation of the whole reactor

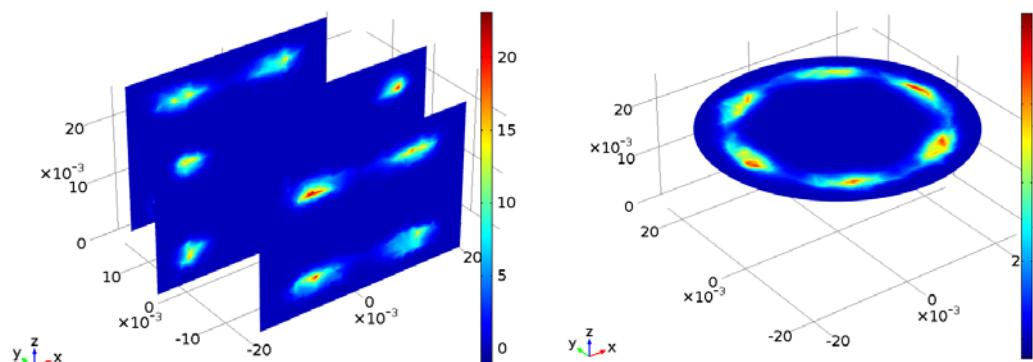


3D thermal field



3D mechanical model
3 basal slip systems α
-> 3 additional ODE for $Nm^{(\alpha)}$

Cylindrical crystal with simple convection cooling on top



Dislocation density increase after 50s cooling / m^{-2}

● Prospects : 3D modeling

Motivation : off-axis orientation of the crystal

2D axisymmetric heat transfer
simulation of the whole reactor

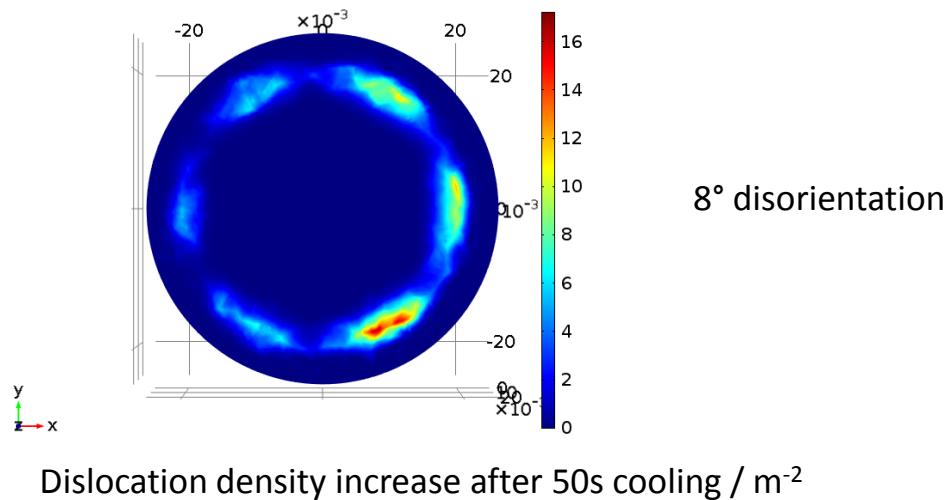


3D thermal field

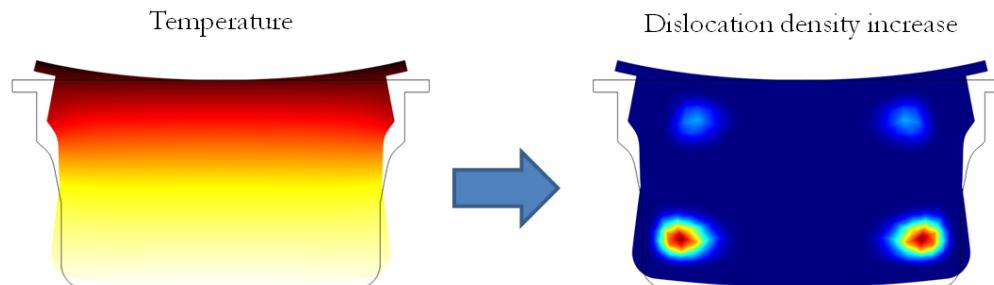


3D mechanical model
3 basal slip systems α
-> 3 additional ODE for $Nm^{(\alpha)}$

Off-axis cylindrical crystal with simple convection cooling on top

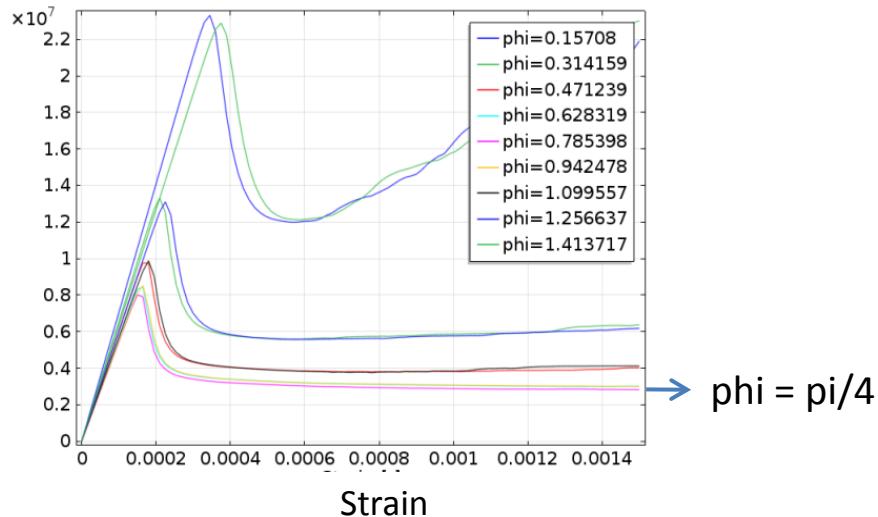


- COMSOL implementation of AH model for crystal plasticity (basal slip systems)
Additional domain ODE + user-defined creep law
- Dislocation density is tracked with an internal variable Nm
- Effect of cooling velocity can be studied
- Two directions for future work : (1) simulation of dislocation increase during growth
(2) 3D modeling for off-axis crystals



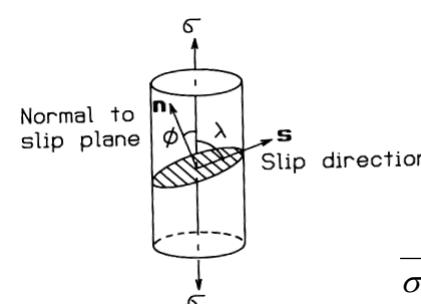
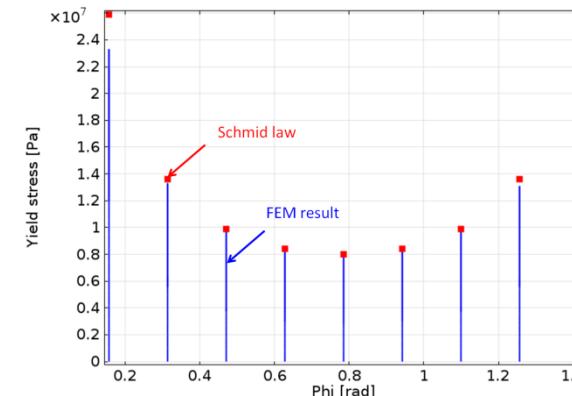
Extra slide : Schmid law

$T = 2300 \text{ K}$



$$\nu_0 = 8.5\text{E}-15; n = 2.8; Q = 3.3\text{eV}; K = 7\text{E}-5; \lambda = 1.1$$

Gao et al., Cryst. Growth Des., 14, 1272-1278 (2014)



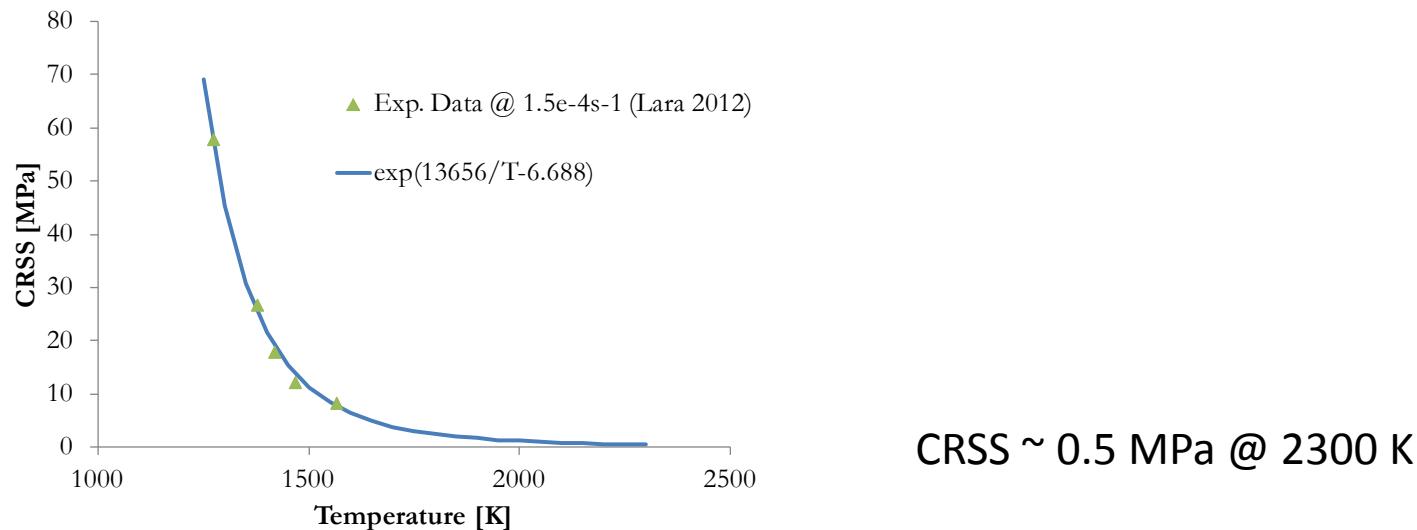
Schmid law

$$\tau = \sigma \cos \phi \cos \lambda$$

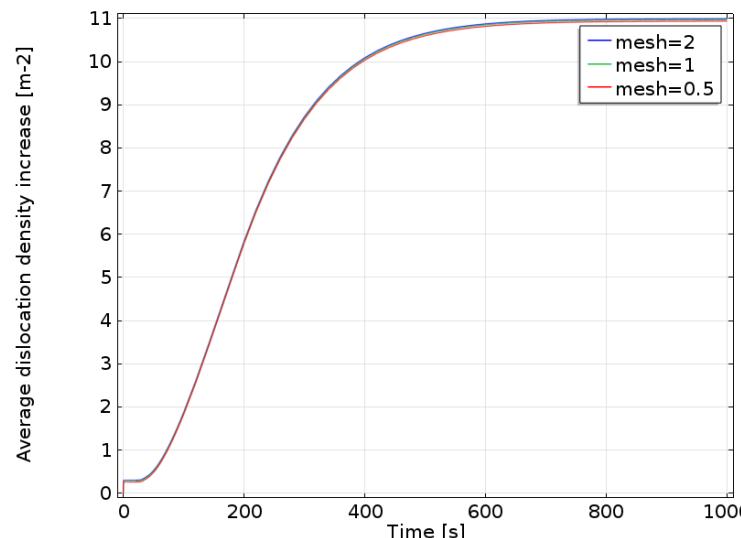
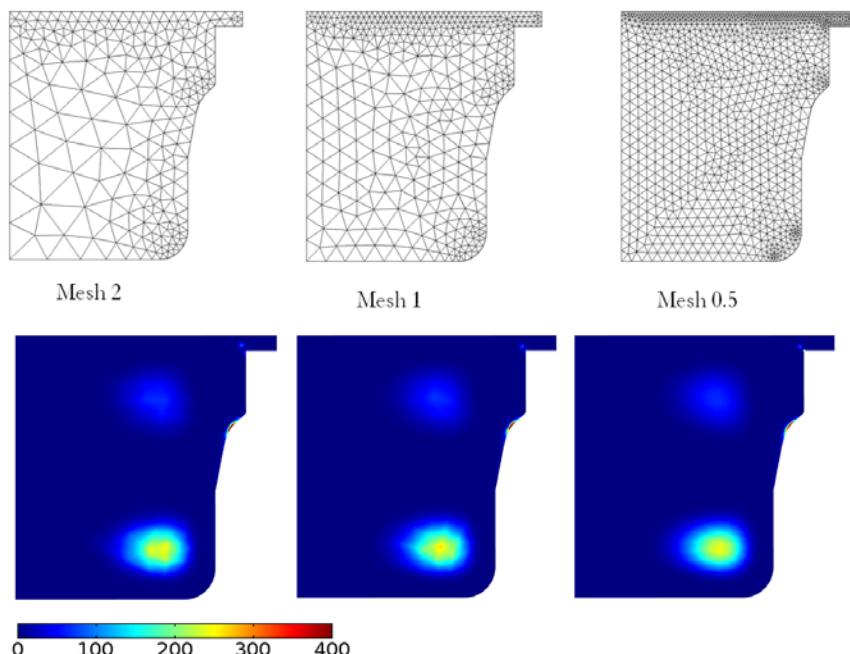


$$\frac{\sigma_{phi}}{\sigma_{phi=\pi/4}} = \frac{1}{2 \cos(phi) \cos(\pi/2 - phi)}$$

Extra slide : CRSS decrease with T

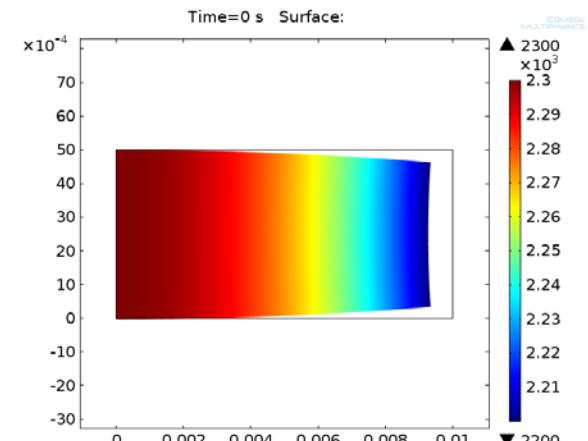
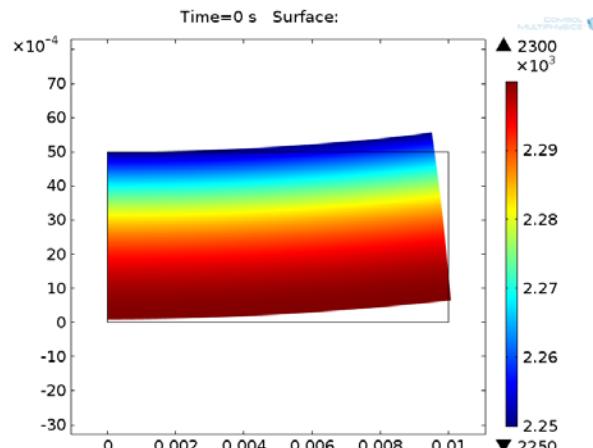


Extra slide : mesh convergence



● Cylindrical crystal

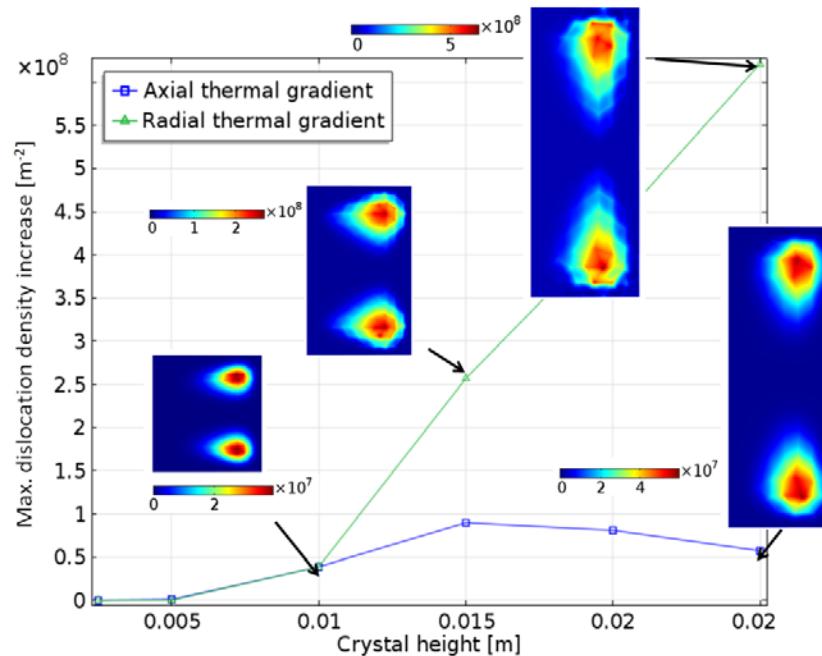
Radial cooling vs axial cooling



Axisymmetric model ; imposed quadratic thermal fields

Cylindrical crystal

Effect of crystal height



Axisymmetric model ; cylindric crystal ; imposed quadratic thermal fields