

A
Design-of-Experiments (DOE)
approach to
FEM Uncertainty Analysis
for optimizing
Magnetic Resonance Imaging
RF Coil Design

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<http://www.nist.gov/itl/math/jeffrey-t-fong.cfm>

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Outline of Talk

(16 slides)

- (4) What is a “Design-of-Experiments” approach ?
- (4) A Design Optimization Problem using FEM (via COMSOL-RF).
- (6) Solution before optimization.
- (1) Solution after optimization.
- (1) Future work.

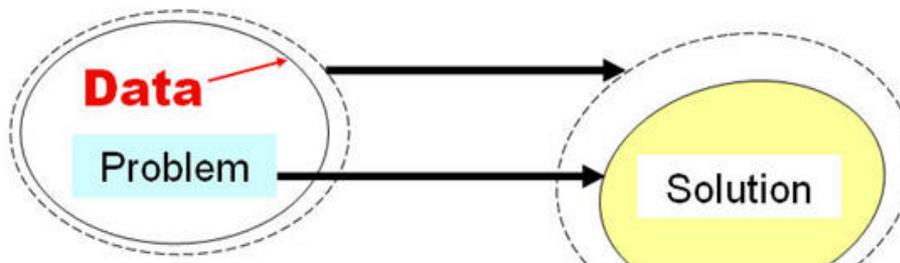
Metrological Approach - “Wiggle each FEM solution”

One “wiggles” an **FEM** solution by varying the input parameters and material property data in a *statistically* rigorous way, i.e., *design of experiments*, to calculate **uncertainty** within an affordable time frame and computing budget.

Such “wiggle” is the 3rd requirement of a “correct” problem:

To be precise, we define a boundary or initial value problem for a partial differential equation, or for a system of partial differential equations, to be *correctly set in the sense of Hadamard* if and only if its solution exists, is unique, and **depends continuously on the data assigned.**

Ref.: Garabedian,
P. R., 1964, *Partial
Diff. Equations*,
page 109.
Providence, RI:
AMS Chelsea
Publishing (1964).



Design of Experiments (*Full vs. Fractional*)

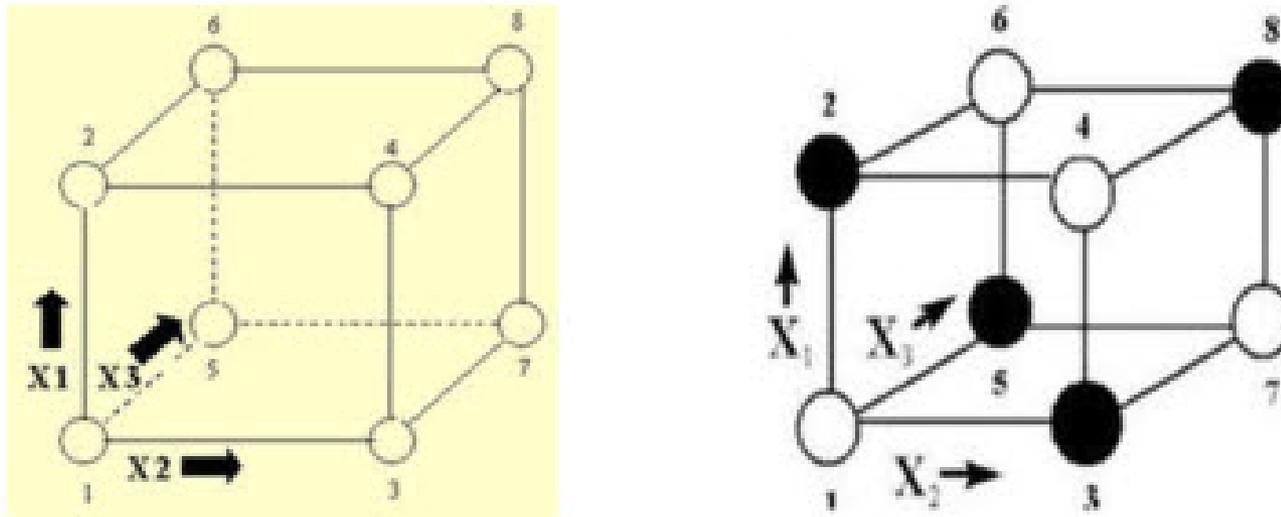
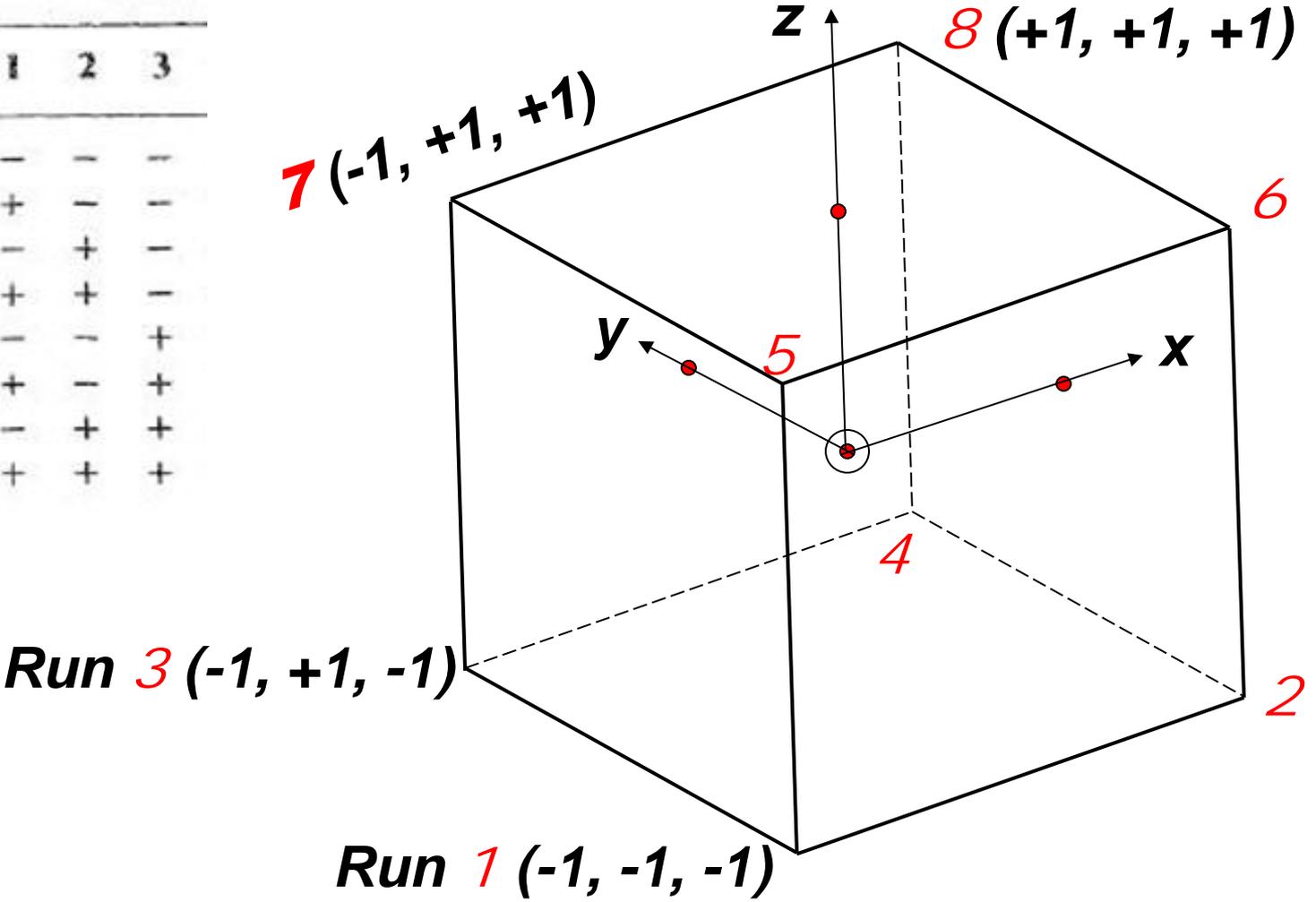


Figure 1. (left) A full-factorial 8-run orthogonal design for 3 factors. (right) A fractional factorial 4-run orthogonal design for 3 factors.

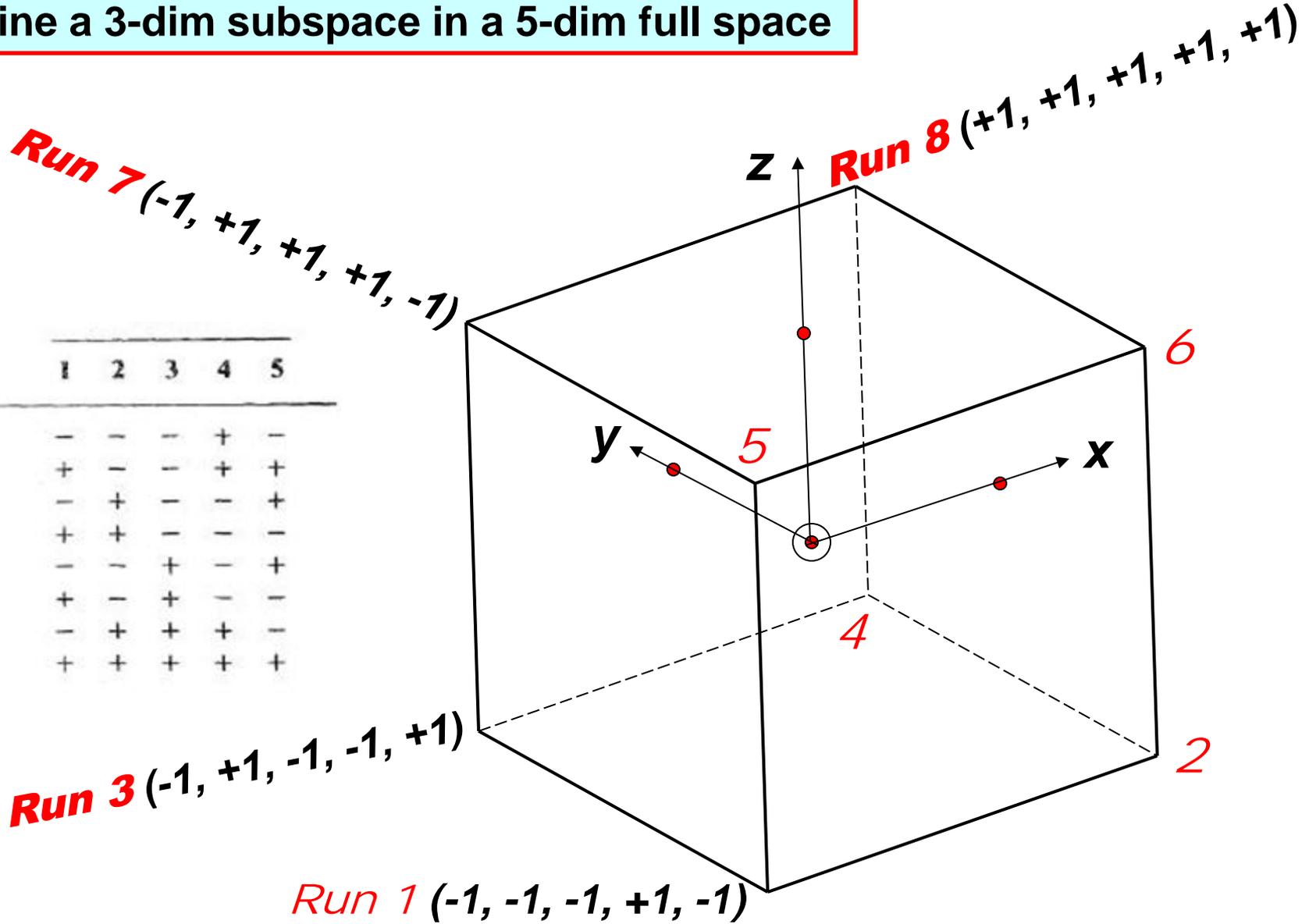
Metrological Approach - "Wiggle each FEM solution"

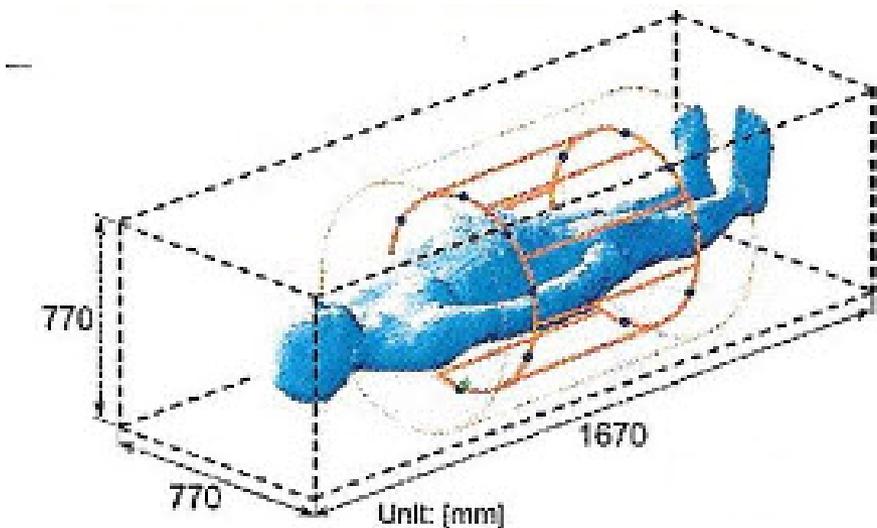
run	1	2	3
1	-	-	-
2	+	-	-
3	-	+	-
4	+	+	-
5	-	-	+
6	+	-	+
7	-	+	+
8	+	+	+



Imagine a 3-dim subspace in a 5-dim full space

run	1	2	3	4	5
1	-	-	-	+	-
2	+	-	-	+	+
3	-	+	-	-	+
4	+	+	-	-	-
5	-	-	+	-	+
6	+	-	+	-	-
7	-	+	+	+	-
8	+	+	+	+	+

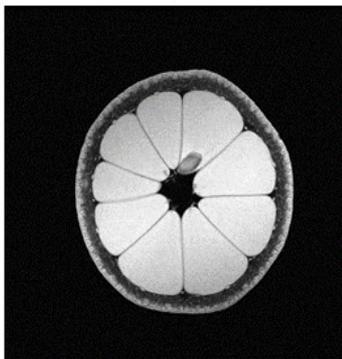
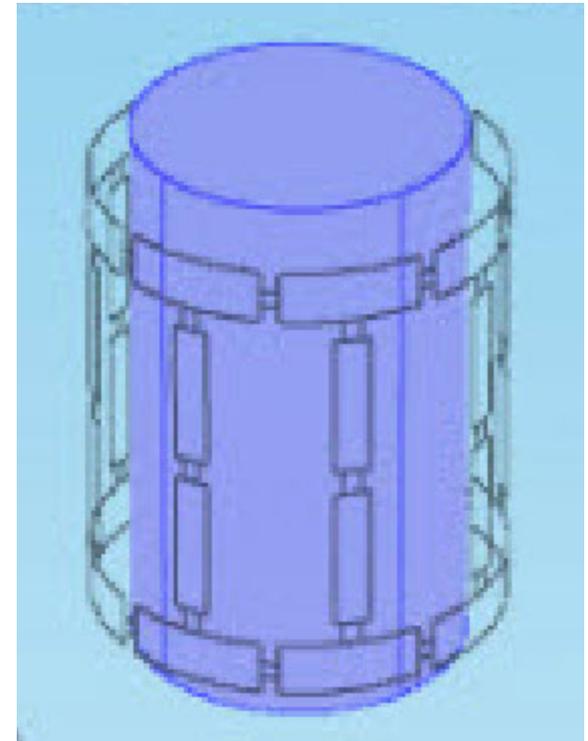
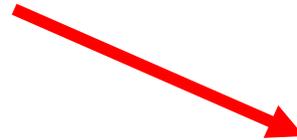
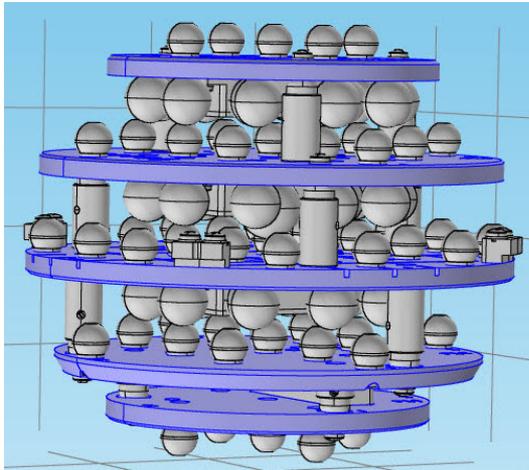




**Motivated
by a
FEM →
project**



A Model Simplification Approach

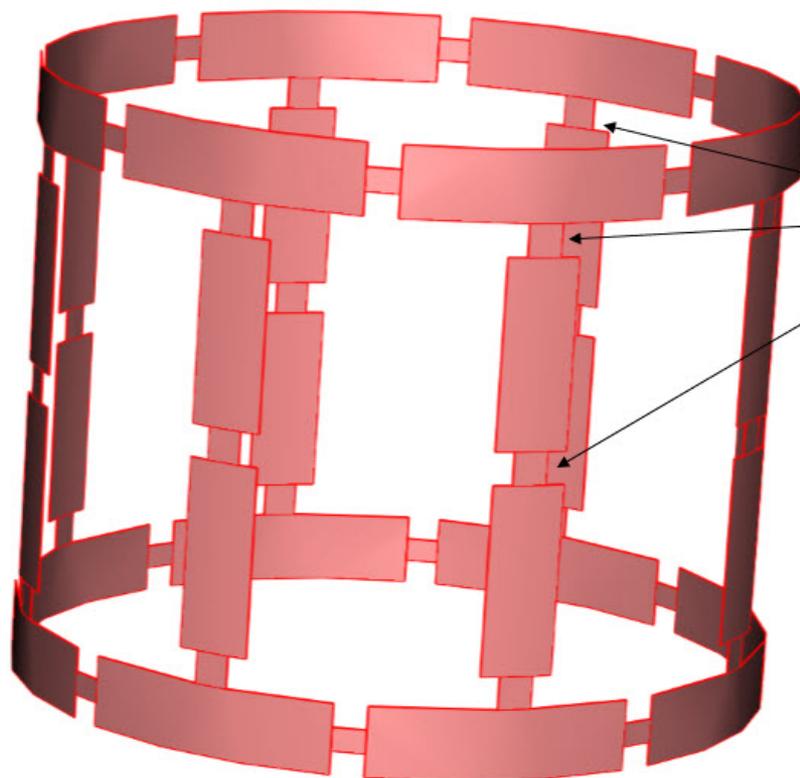


MRI image of a lemon
(Courtesy of Dr. Steve Russek
NIST, Boulder CO 80305)



MRI image of a banana
(Courtesy of Dr. Steve Russek
NIST, Boulder CO 80305)

- MRI



Each flap represents a simple circuit or port element such as a 50 Ohm feed or a tuning capacitor.

(Standard finite element modeling approach for RF and Microwave components)

$$\nabla \times \mu_r^{-1}(\nabla \times \mathbf{E}) - k_0^2 \left(\epsilon_r - \frac{j\sigma}{\omega\epsilon_0} \right) \mathbf{E} = 0$$

COMSOL
RF module

$$\nabla \times \mu_r^{-1}(\nabla \times \mathbf{E}) - k_0^2(\epsilon_r - \frac{j\sigma}{\omega\epsilon_0})\mathbf{E} = 0$$

$$\nabla \times \mathbf{E} = i\omega \mathbf{B}$$

Norm (B) = RMS (B).

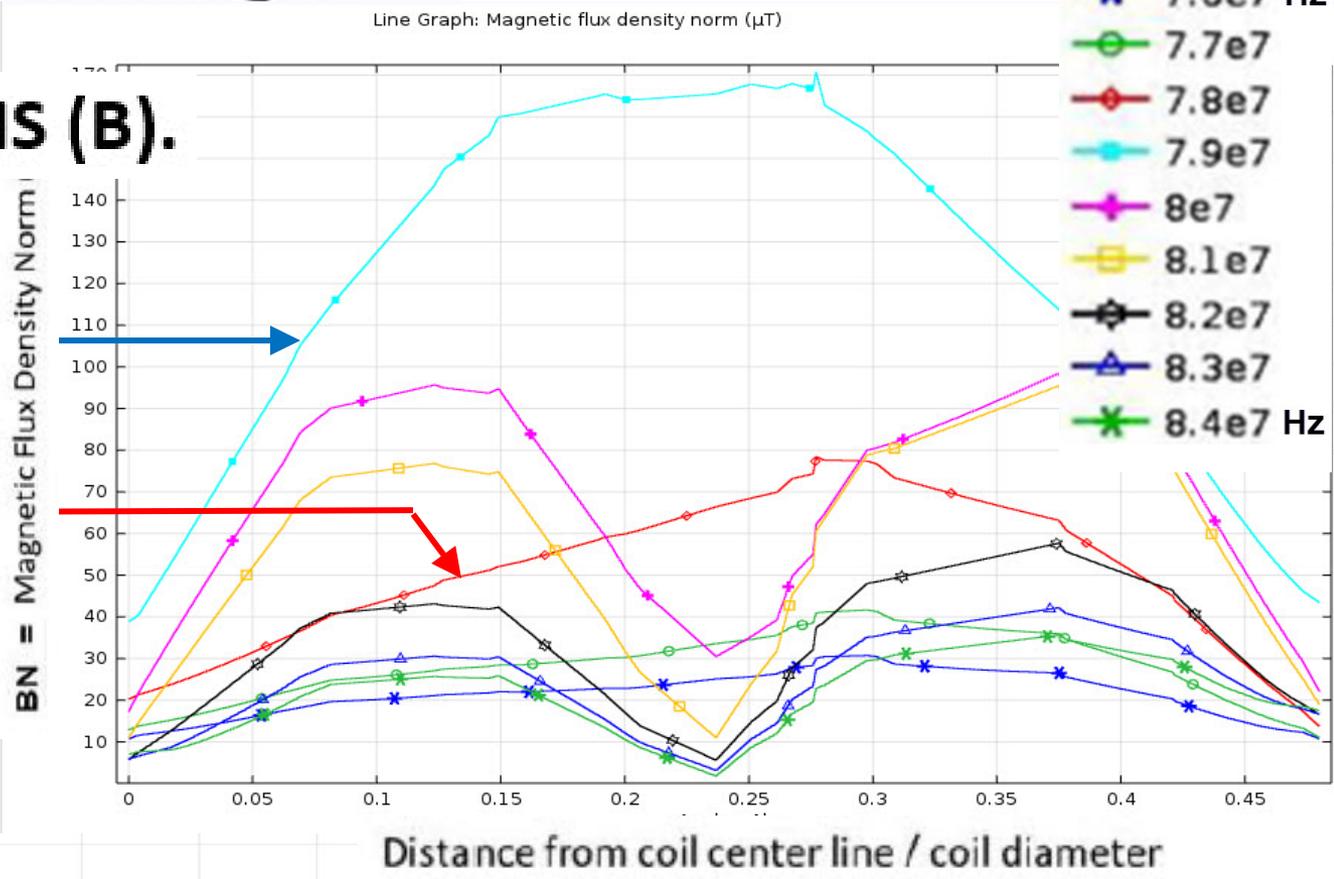
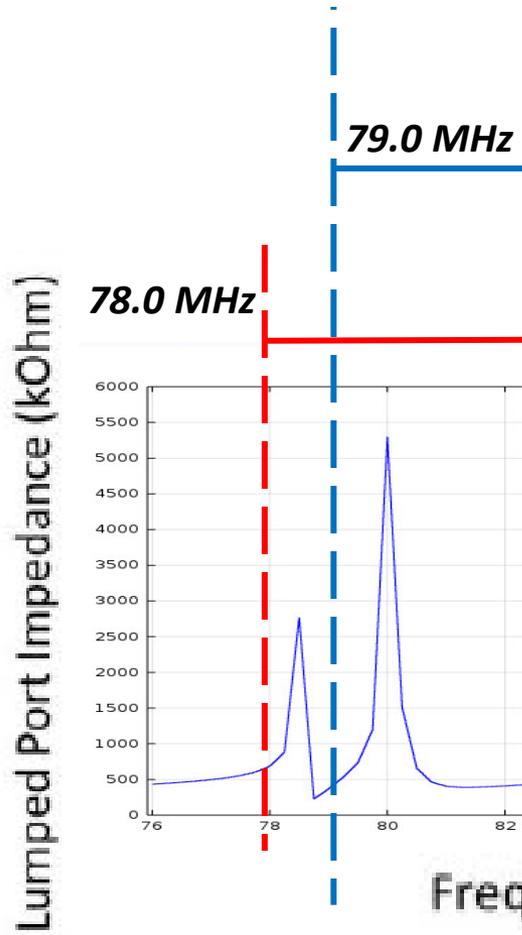
Quantity	Value/Expression	Unit	Description
Boundary condition:	Scattering boundary condition		
Incident: field:	Wave given by E field		
E_0	0 0 0	V/m	Electric field
Wave type:	Spherical wave		
\mathbf{k}	-nx_rfw -ny_rfw -nz_rfw	1	Wave direction
\mathbf{r}_0	0 0 0	m	Source point

The sphere has a Scattering boundary conditions = non-reflecting.
A refined model would, in addition, add a Perfectly Matched Layer for more precise absorption.

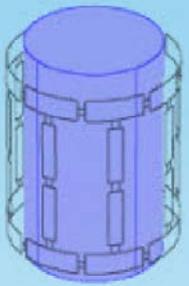
$$\nabla \times \mu_r^{-1}(\nabla \times \mathbf{E}) - k_0^2(\epsilon_r - \frac{j\sigma}{\omega\epsilon_0})\mathbf{E} = 0$$

$$\nabla \times \mathbf{E} = i\omega \mathbf{B}$$

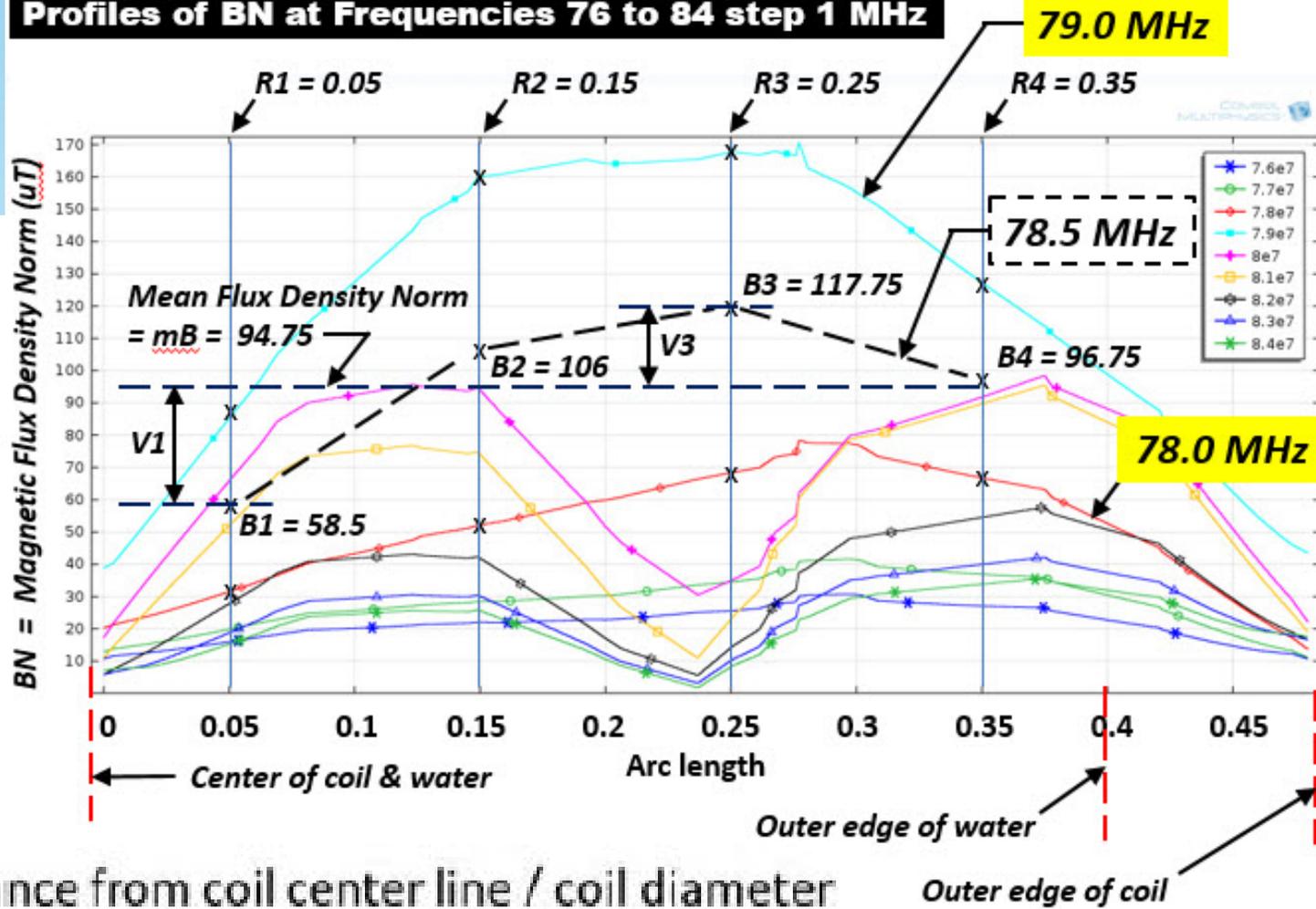
$$\text{Norm}(\mathbf{B}) = \text{RMS}(\mathbf{B}).$$



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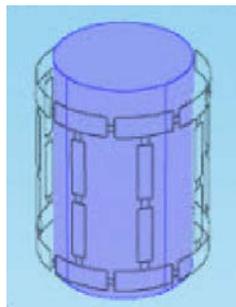


Profiles of BN at Frequencies 76 to 84 step 1 MHz



Distance from coil center line / coil diameter

Outer edge of coil



X1	X2	X3	X4	X5	X6	X7
-1	-1	-1	+1	+1	+1	-1
+1	-1	-1	-1	-1	+1	+1
-1	+1	-1	-1	+1	-1	+1
+1	+1	-1	+1	-1	-1	-1
-1	-1	+1	+1	-1	-1	+1
+1	-1	+1	-1	+1	-1	-1
-1	+1	+1	-1	-1	+1	-1
+1	+1	+1	+1	+1	+1	+1
+1	+1	+1	-1	-1	-1	+1
-1	+1	+1	+1	+1	-1	-1
+1	-1	+1	+1	-1	+1	-1
-1	-1	+1	-1	+1	+1	+1
+1	+1	-1	-1	+1	+1	-1
-1	+1	-1	+1	-1	+1	+1
+1	-1	-1	+1	+1	-1	+1
-1	-1	-1	-1	-1	-1	-1

	X1	X2	X3	X4	X5	X6	X7
	Sigma	Epsilon _r	C	V0	w1	L3	bet2
Base Run (00)	0.0001	80	177	500	80	35	5
Unit	S/m	l	pF	volt	mm	mm	degree
+ / - variation	10 %	5 %	2 %	2 %	5 %	10 %	10 %
Run No. (01)	0.00009	76	173.46	510	84	38.5	4.5
Run No. (02)	0.00011	76	173.46	490	76	38.5	5.5
Run No. (03)	0.00009	84	173.46	490	84	31.5	5.5
Run No. (04)	0.00011	84	173.46	510	76	31.5	4.5
Run No. (05)	0.00009	76	180.54	510	76	31.5	5.5
Run No. (06)	0.00011	76	180.54	490	84	31.5	4.5
Run No. (07)	0.00009	84	180.54	490	76	38.5	4.5
Run No. (08)	0.00011	84	180.54	510	84	38.5	5.5
Run No. (09)	0.00011	84	180.54	490	76	31.5	5.5
Run No. (10)	0.00009	84	180.54	510	84	31.5	4.5
Run No. (11)	0.00011	76	180.54	510	76	38.5	4.5
Run No. (12)	0.00009	76	180.54	490	84	38.5	5.5
Run No. (13)	0.00011	84	173.46	490	84	38.5	4.5
Run No. (14)	0.00009	84	173.46	510	76	38.5	5.5
Run No. (15)	0.00011	76	173.46	510	84	31.5	5.5
Run No. (16)	0.00009	76	173.46	490	76	31.5	4.5

760file1.txt - Notepad

File Edit Format View Help

```

Filename: 760file1.txt Date: June 25,
Num of Factors
7
factors
X1 X2 X3 X4 X5 X6 X7
key to factors
X factor name symbol (on a new line)
Elec. Conductivity of Water
sigma
Relative Permittivity of Water
epsilon
Capacitance
C
Voltage
V0
Ring Width
w1
Strip Gap Length
L3
Ring Gap Angle
bet2
center Point values
0.0001 80 177 500 80 35 5
variability (%)
10.0 5.0 2.0 2.0 5.0 10.0 10.0
    
```

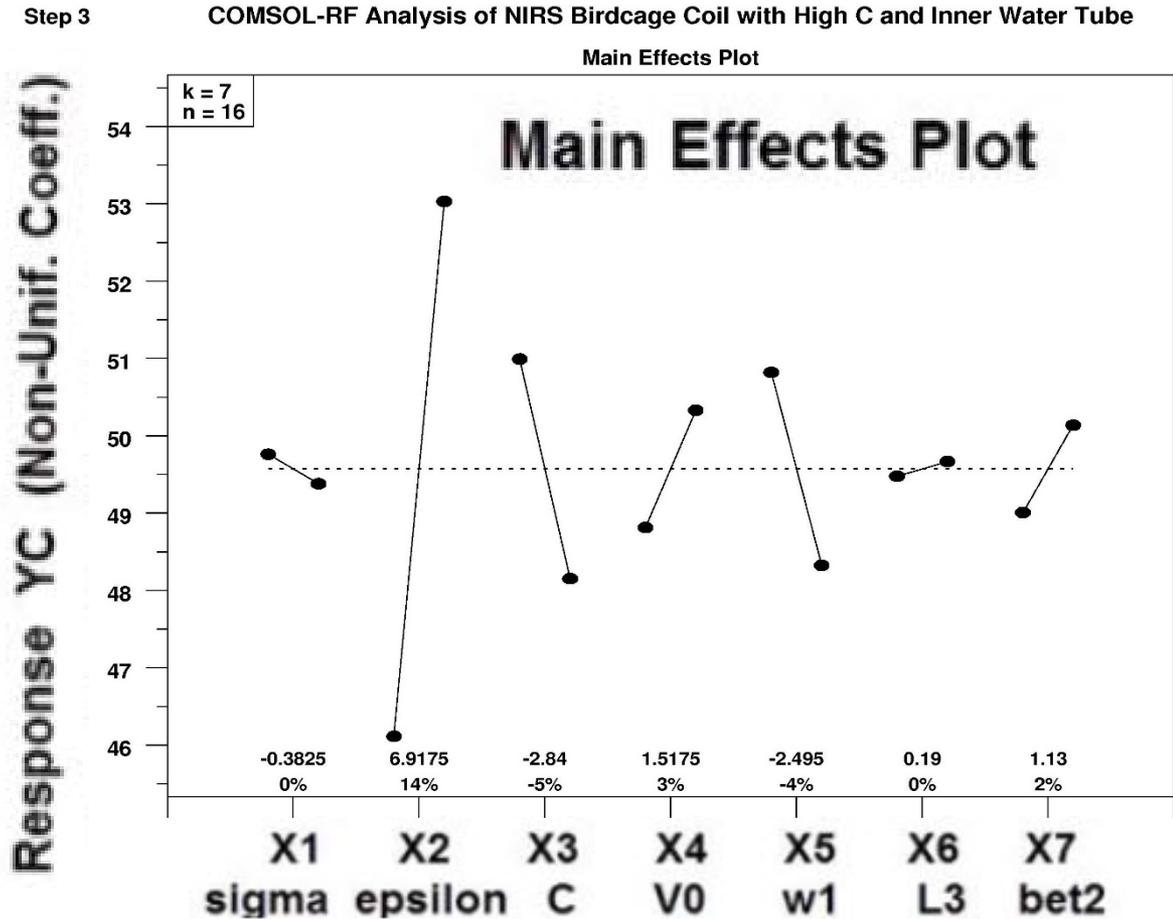
760file2.txt - Notepad

File Edit Format View Help

```

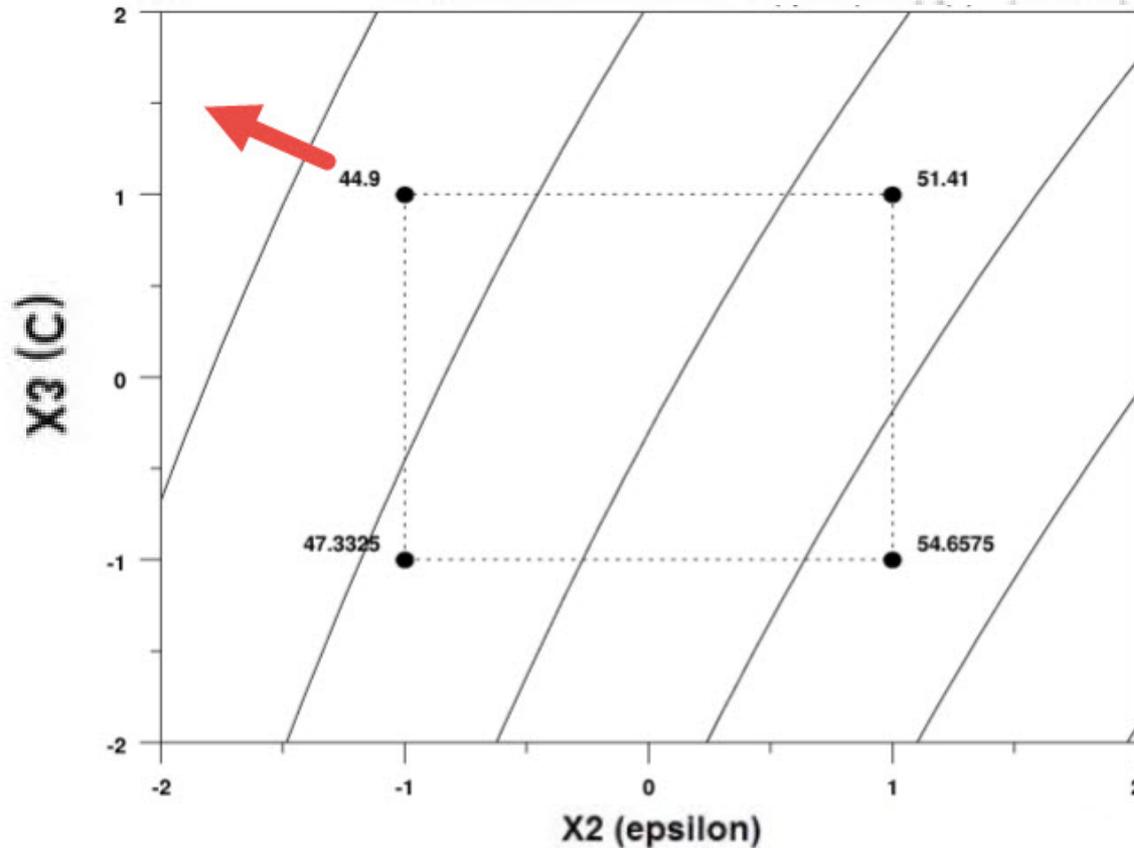
Filename: 760file2.txt Date: Aug. 10, 2014
Num of Factors
7
num of runs
8 16
num of runs chosen for DOE
16
runs number
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16
key to results
YC result name symbol (next line)
Non-Uniformity Coeff.
YC
results for runs
46.89
42.92 49.28 52.17 57.99 43.01 44.73 50.58 54.25
48.95 51.86 45.52 46.34 47.85 60.62 46.50 50.63
    
```

DATAPLOT



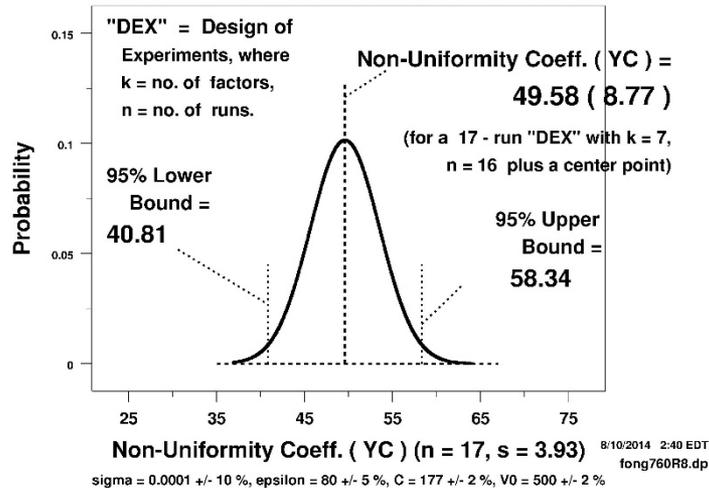
DATAPLOT

Step 10 **Contour Plot of the 2-Dominant Factors: X2 (epsilon) and X3 (C)**

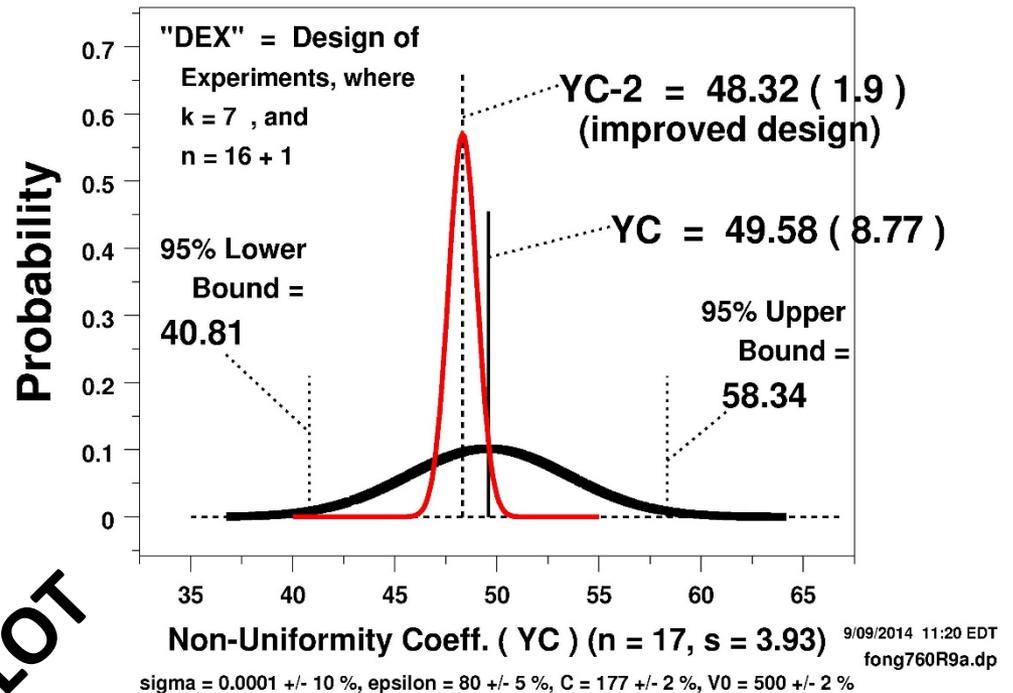


Predicted	$y(0,0) = \bar{y}$	= 49.575
Data	$y(0,0)$	= 46.89

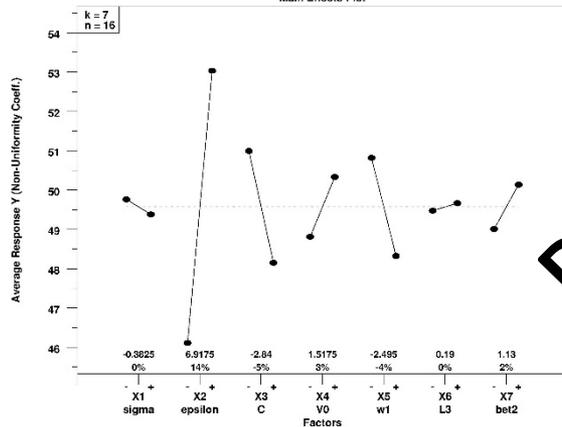
Non-Uniformity of NIRS Coil Magnetic Flux Density in Inner Water Tube
95% Uncertainty Bounds Plot with Dataplot (Fong-Stupic-Keenan-Russek, 2014)



Non-Uniformity of NIRS Coil Magnetic Flux Density in Inner Water Tube
95% Uncertainty Bounds Plot with Dataplot (Fong-Stupic-Keenan-Russek, 2014)



Step 3 COMSOL-RF Analysis of NIRS Birdcage Coil with High C and Inner Water Tube
Main Effects Plot



DATAPLOT

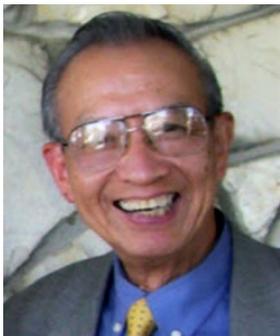
Before:
 $NUC = 49.58 (8.77)$
After:
 $NUC = 48.32 (1.90)$

Future Work

- 1. A new model with geometry and physics comparable to an actual coil.*
- 2. Application of the DOE approach to the new model.*
- 3. Experimental verification of the newly-optimized model.*

Disclaimer

Certain commercial equipment, instruments, materials, or computer software are identified in this talk in order to specify the experimental or computational procedure adequately. Such identification is not intended to imply recommendation or endorsement by the National Institute of Standards & Technology, nor is it intended to imply that the materials, equipment, or software identified are necessarily the best available for the purpose.



Dr. Jeffrey T. Fong has been Physicist and Project Manager at the Applied and Computational Mathematics Division, Information Technology Laboratory, National Institute of Standards and Technology (NIST), Gaithersburg, MD, since 1966.

He was educated at the University of Hong Kong (B.Sc., Engineering, first class honors, 1955), Columbia University (M.S., Engineering Mechanics, 1961), and Stanford (Ph.D., Applied Mechanics and Mathematics, 1966). Prior to 1966, he worked as a design engineer (1955-63) on numerous power plants (hydro, fossil-fuel, nuclear) at Ebasco Services, Inc., in New York City, and as teaching & research assistant (1963-66) on engineering mechanics at Stanford University.

During his 40+ years at NIST, he has conducted research, provided consulting services, and taught numerous short courses on mathematical and computational modeling with uncertainty estimation **for fatigue, fracture, high-temperature creep, nondestructive evaluation, electromagnetic behavior, and failure analysis of a broad range of materials ranging from paper, ceramics, glass, to polymers, composites, metals, semiconductors, and biological tissues.**

A licensed professional engineer (P.E.) in the State of New York since 1962 and a chartered civil engineer in the United Kingdom and British Commonwealth (A.M.I.C.E.) since 1968, he has authored or co-authored more than 100 technical papers, and edited or co-edited 17 national or international conference proceedings. He was elected Fellow of ASTM in 1982 and Fellow of ASME in 1984. In 1993, he was awarded the prestigious ASME *Pressure Vessels and Piping Medal*. Most recently, he was honored at the 2014 International Conference on Computational & Experimental Engineering & Sciences (ICCES) with a *Lifetime Achievement Medal*.

Since 2006, he has been Adjunct Professor of Mechanical Engineering and Mechanics at Drexel University and taught a graduate-level 3-credit course on “Finite Element Method Uncertainty Analysis.” Since Jan. 2010, he has given every 6 months an on-line 3-hour short course at Stanford University on “Reliability and Uncertainty Estimation of FEM Models of Composite Structures.” In 2012, he was appointed Adjunct Professor of Nuclear and Risk Engineering at the City University of Hong Kong, and Distinguished Guest Professor at the East China University of Science & Technology, Shanghai, China, to teach annually a 1-credit 16-hour short course on “Engineering Reliability and Risk Analysis.”