

Phase-field Method in Analysis of Nanocomposite Morphological Stability

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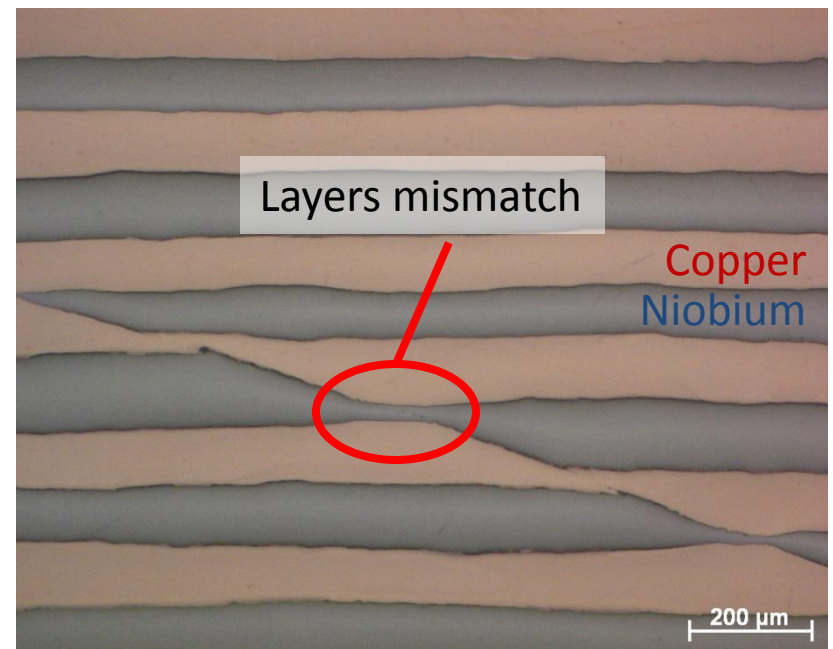
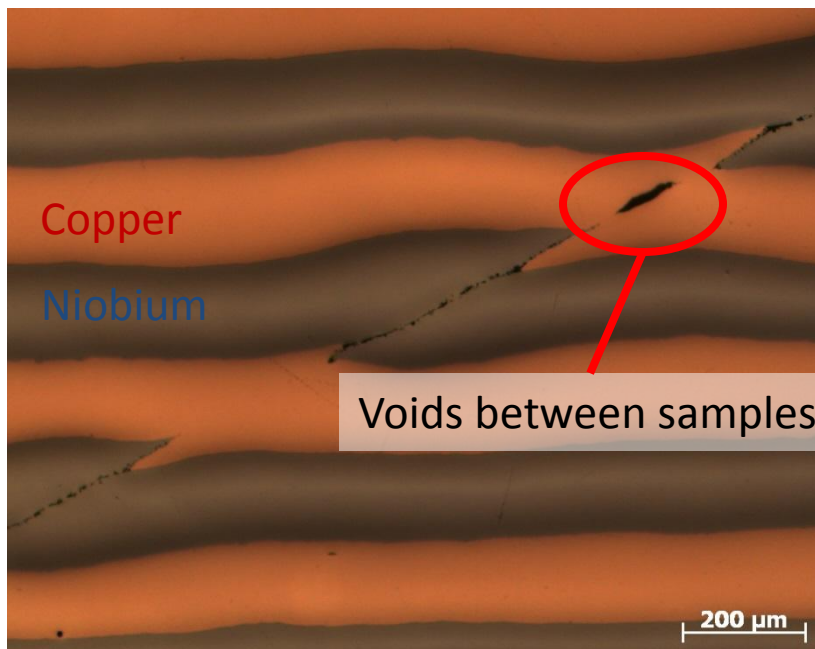


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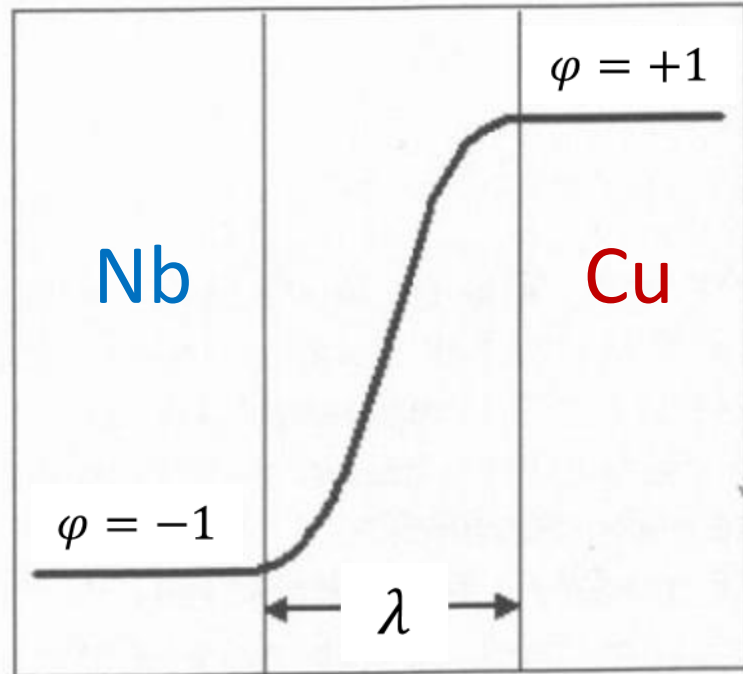
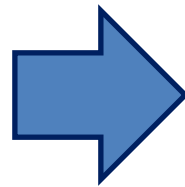
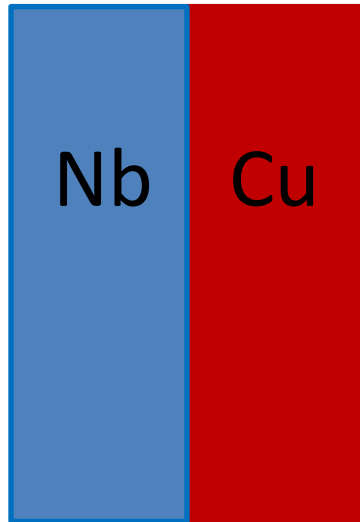
Problem of joining defects

Joining method of choice: diffusion welding

Question: are the welding defects stable under exposure to high temperature and pressure for extended periods of time?



Phase-field method equations



Cahn-Hilliard equation for phase separation:

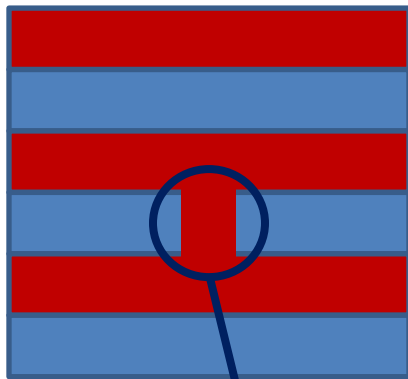
$$\frac{\partial \phi(\vec{r}, t)}{\partial t} = M \nabla^2 (-W_0 \nabla^2 \phi + H(\phi^3 - \phi))$$

COMSOL: coefficient form set of two PDEs

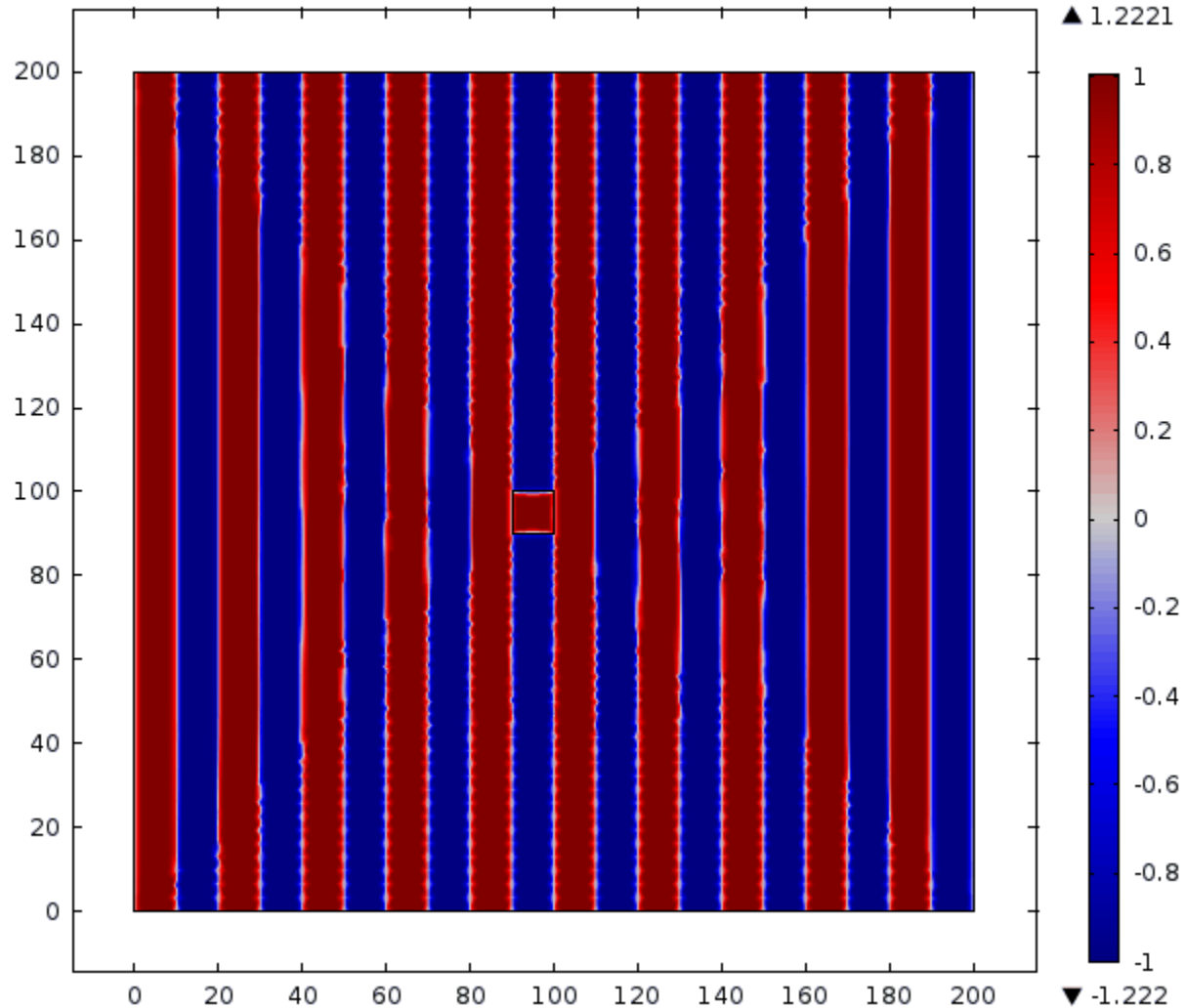
2D pinched layer instability

Time=0 Surface: Dependent variable u

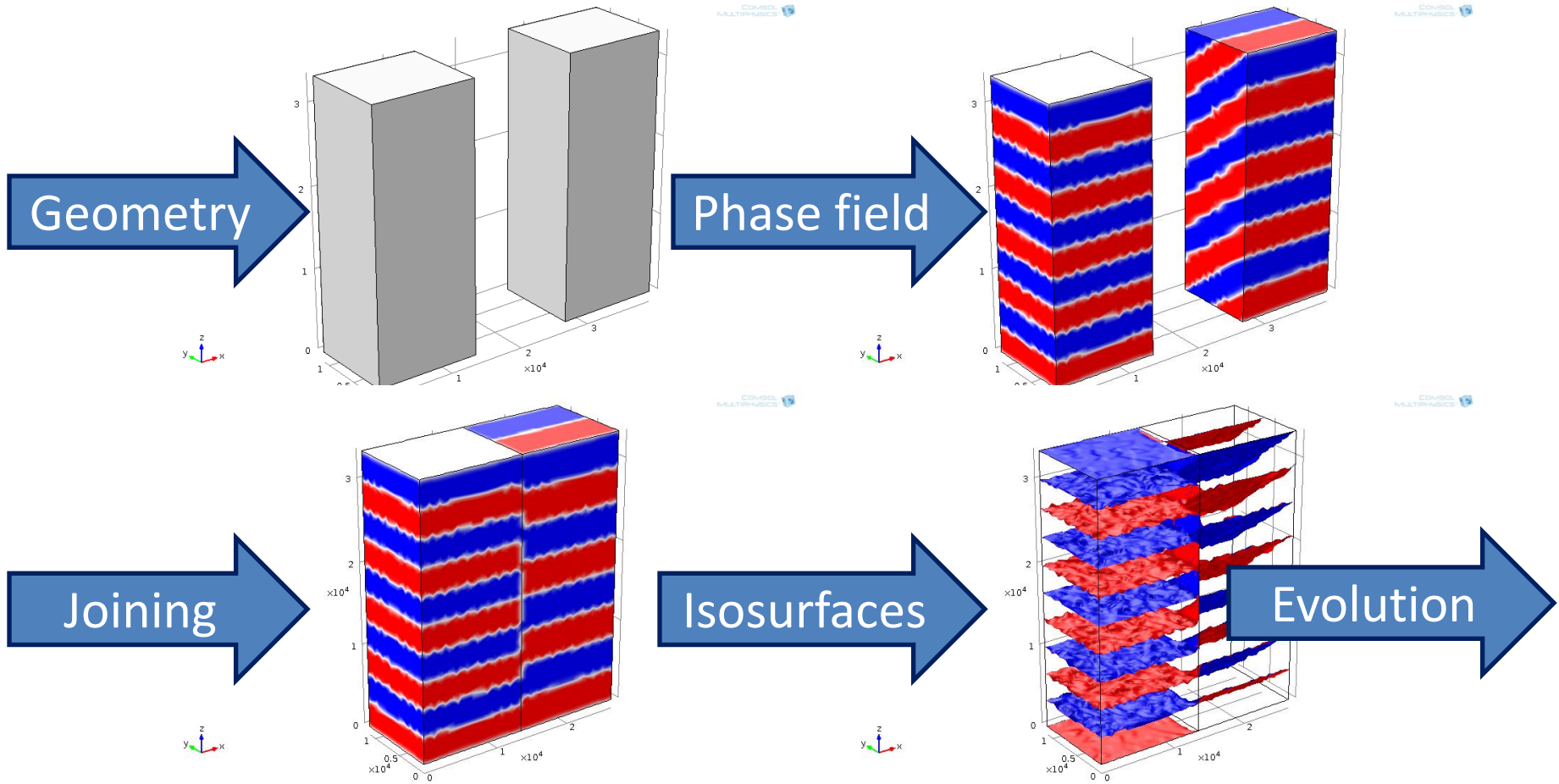
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Cu pinchoff



Model construction

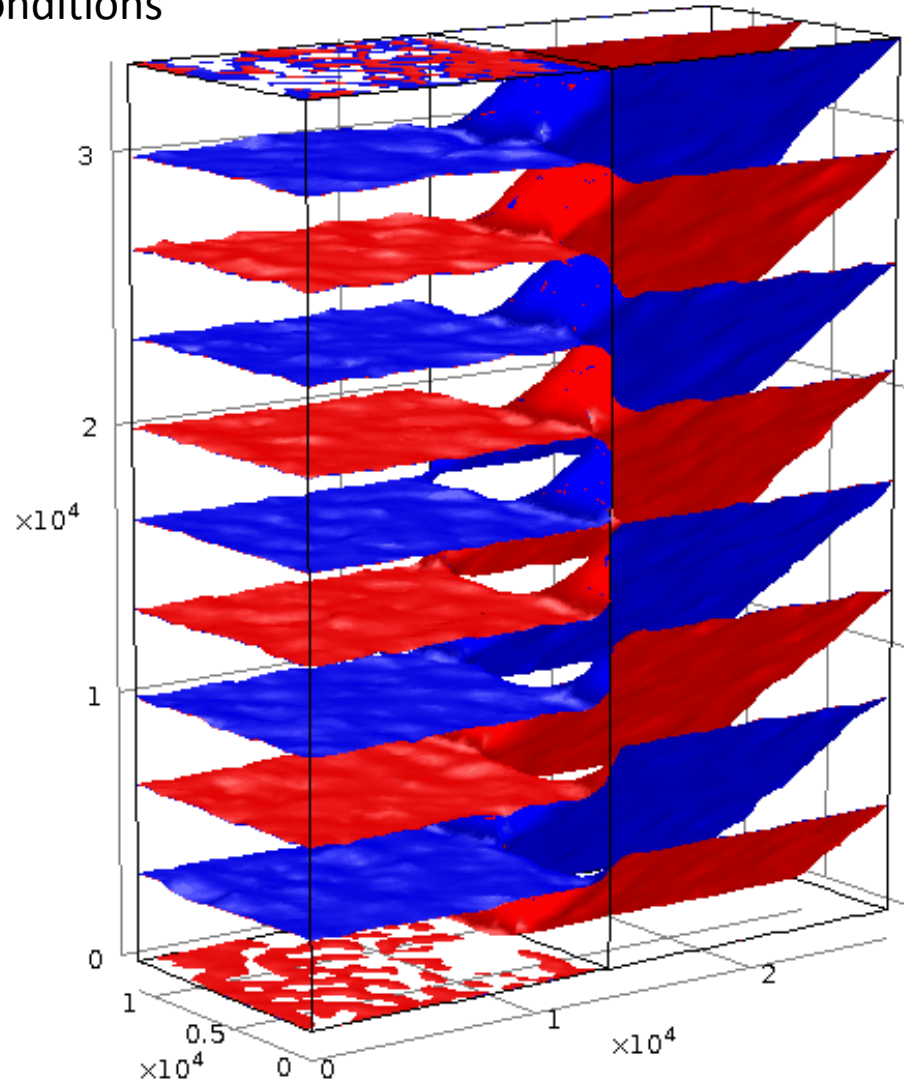
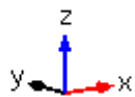


Twist defect

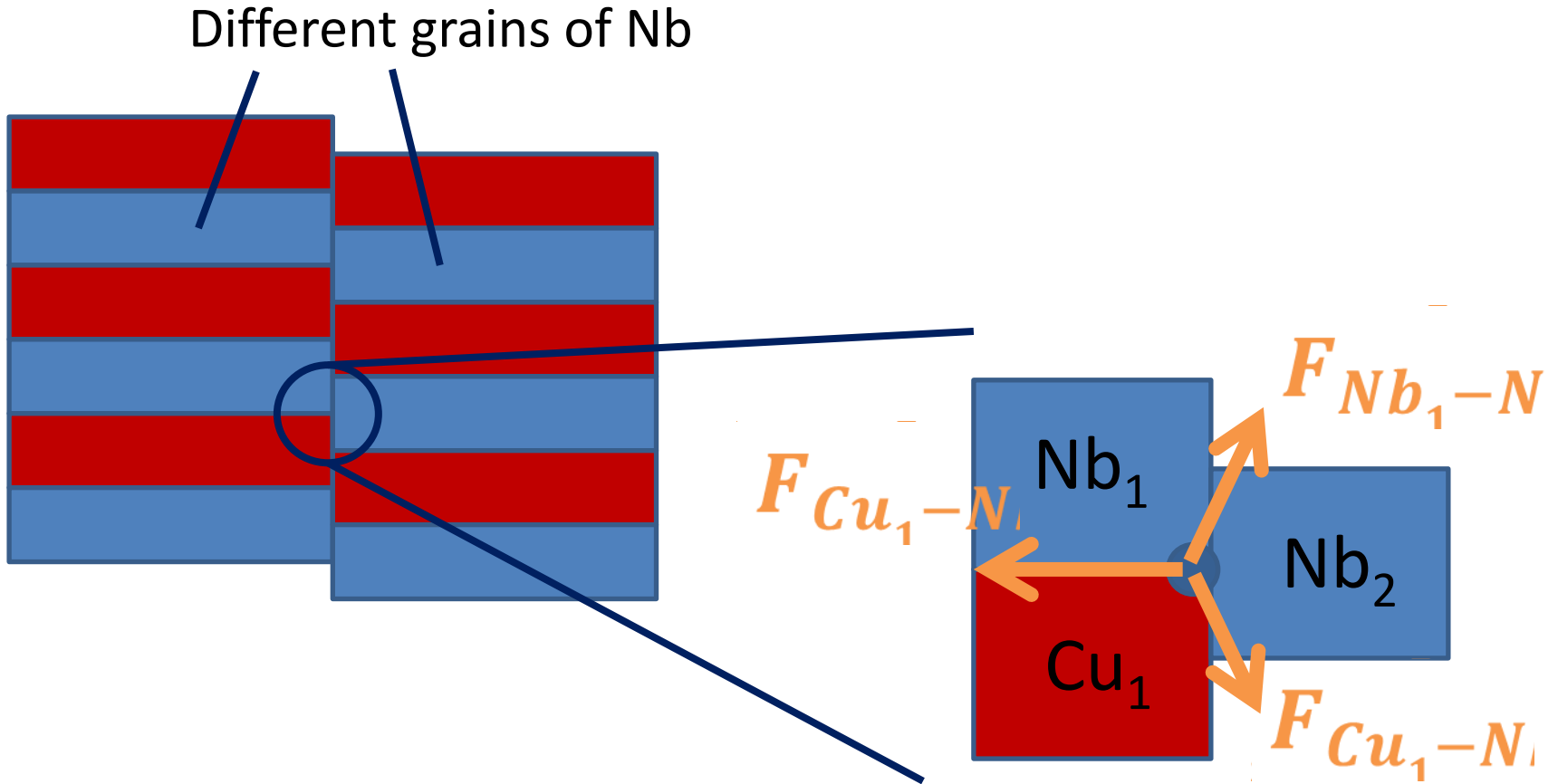
Time=0 Isosurface: Dependent variable u2

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- Periodic boundary conditions in y, z directions



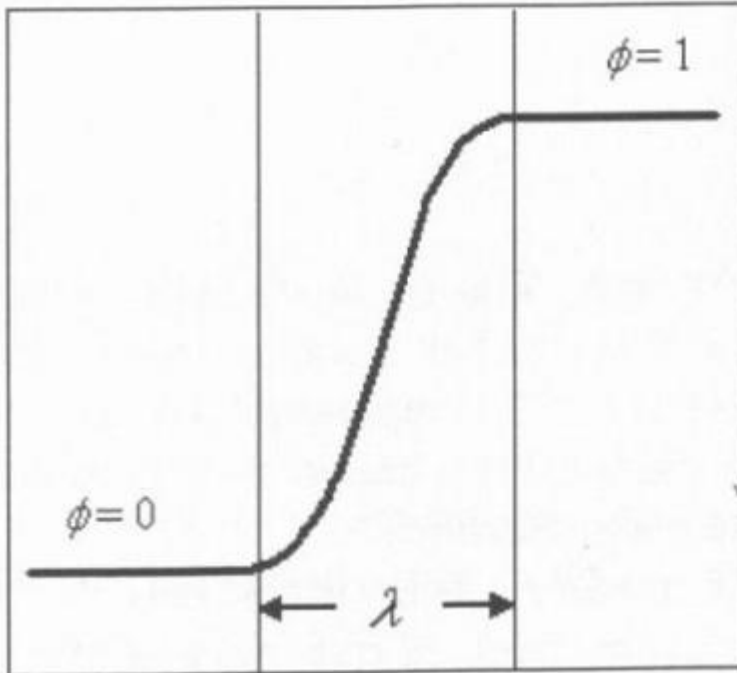
Inclusion of grain boundaries



Conclusions

- Phase-field model provides robust and accurate predictions of behavior of nanocomposite phase interfaces.
- Instability and indefinite collapse of layers is proven to be a typical feature of diffusion joints in 2D and 3D for single-phase-field model.
- It may be possible to hinder joining instabilities by incorporating the boundaries between the adjacent grains into the model

Phase-field method introduction



- Sharp interfaces are replaced with continuous phase-field with some normalization
- Free energy of the composite calculated in every point
- System tries to minimize free energy, which is manifested in the equations of motion
- Balance of Cu-Nb is maintained as a conserved order parameter

Free energy:

$$F = \int [f(\varphi) + \frac{\alpha}{2} (\nabla\varphi)^2] d^3r$$


Bulk energy


Interface energy

Phase-field method equations

Cahn-Hilliard equation for phase separation:

$$\frac{\partial \varphi(\vec{r}, t)}{\partial t} = M \nabla^2 \left(-W_0 \nabla^2 \varphi + \frac{\partial g}{\partial \varphi} \right)$$

Double-well potential:

$$g(\varphi) = H \left(\frac{\varphi^4}{4} - \frac{\varphi^2}{2} \right)$$

COMSOL implementation:

coefficient form set of PDEs (two PDEs for each conserved order parameter)

Allows easy expansion to include multiple order parameters

Equation

Show equation assuming:

Study 1, Time Dependent

$$e_a \frac{\partial^2 \mathbf{u}}{\partial t^2} + d_a \frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (-c \nabla \mathbf{u} - \alpha \mathbf{u} + \gamma) + \beta \cdot \nabla \mathbf{u} + \alpha \mathbf{u} = f$$

$\mathbf{u} = [u, v]^T$

$\nabla = \left[\frac{\partial}{\partial x}, \frac{\partial}{\partial y} \right]$

Diffusion Coefficient

0 M

Isotropic Isotropic

c

-Wu 0

Isotropic Isotropic

Absorption Coefficient

0 0

a

-2.6*H*(u*u-1) 1

Source Term

Mass Coefficient

Damping or Mass Coefficient

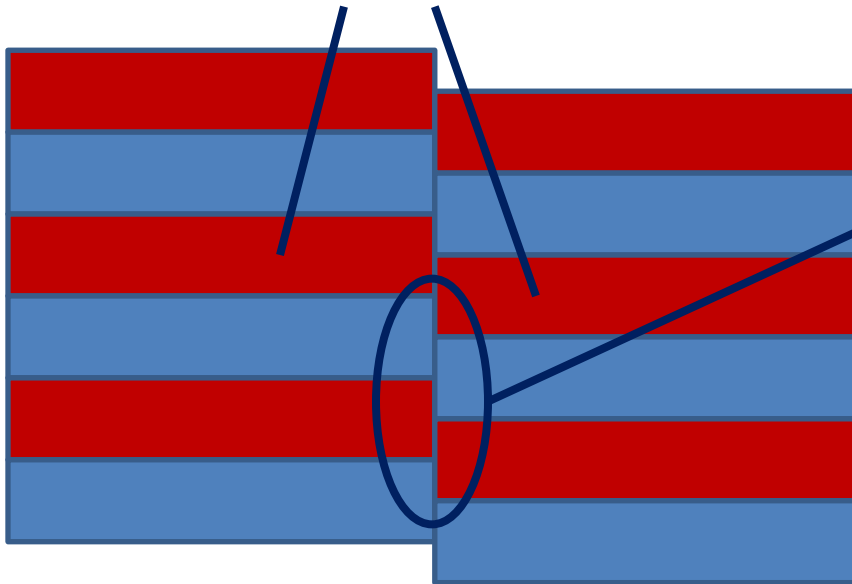
1 0

d_a

0 0

Inclusion of grain boundaries

Different grains of Cu



Can extra grain boundaries stabilize the joint?

Conserved order parameter

Cu-Nb field

two 2nd-order PDEs
(Cahn-Hilliard eqn)



Non-conserved order parameter

Cu 1st grain/Nb 1st grain
Cu 2nd grain/Nb 2nd grain

...

one 2nd-order PDE
per used grain
(Allen-Cahn eqn)