



# IMPROVEMENT OF A STEADY STATE METHOD OF THERMAL INTERFACE MATERIAL CHARACTERIZATION BY USE OF A THREE DIMENSIONAL FEA SIMULATION IN COMSOL MULTIPHYSICS

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# PROBLEM STATEMENT

✓ Problem

Statement

- Background
- Methodology
- COMSOL Model
- Mesh
- Results
- Concluding Remarks

- The Lab of Applied Multiphase Thermal Engineering at Dalhousie University has a contract with Raytheon to work on the characterization of thermal interface materials (TIMs).
- The first step in the project was to build and test a steady state characterization device.
- The goal of the work presented here was to create an FEA simulation of that test device which could be used to improve the accuracy of the experiment.



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- What are Thermal Interface Materials?
  - Materials which are designed to increase the thermal conductance of an interface between two surfaces.
  - A common application is to reduce resistance of the conduction path from a microchip to a heat sink.

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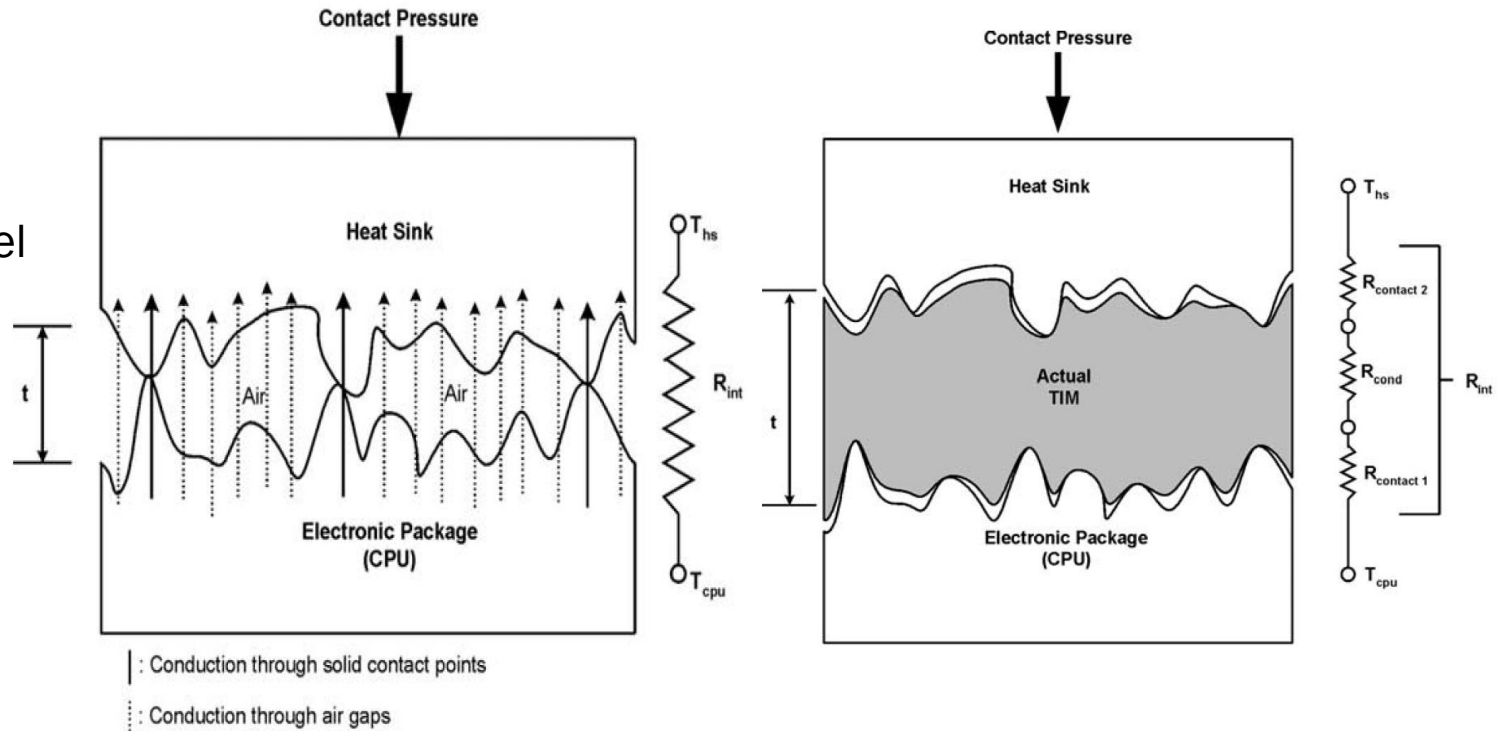


Illustration of contact resistance [1]



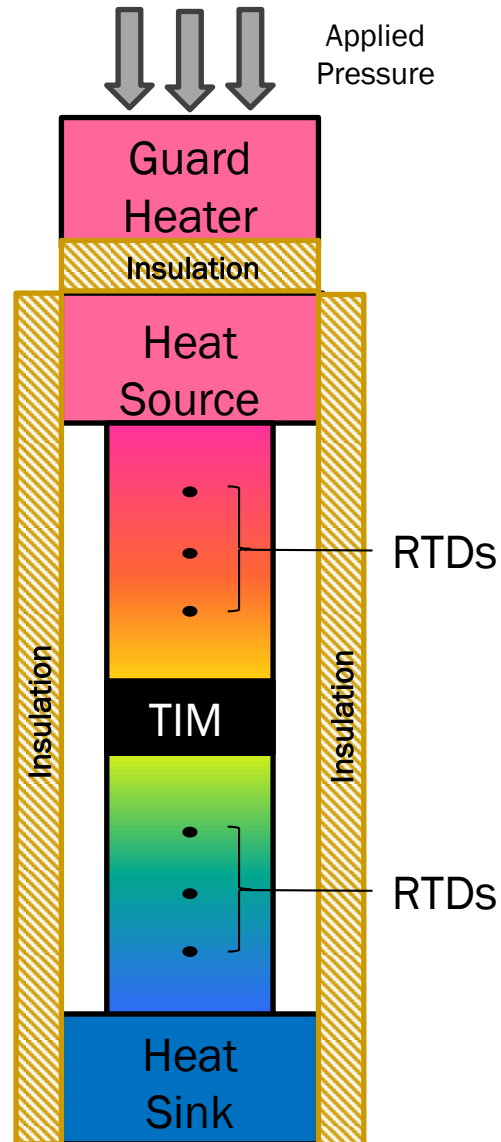
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- The performance of a TIM is a function of:
    - Effective thermal conductivity
    - Ability to conform to surface features
    - Thickness of the TIM layer
  - It is not possible to characterize the performance of a TIM with a single property such as bulk thermal conductivity.
  - Roughness and surface flatness are important parameters
  - Performance will vary with both clamping pressure and TIM temperature
  - We must measure its performance while it is in an interface.



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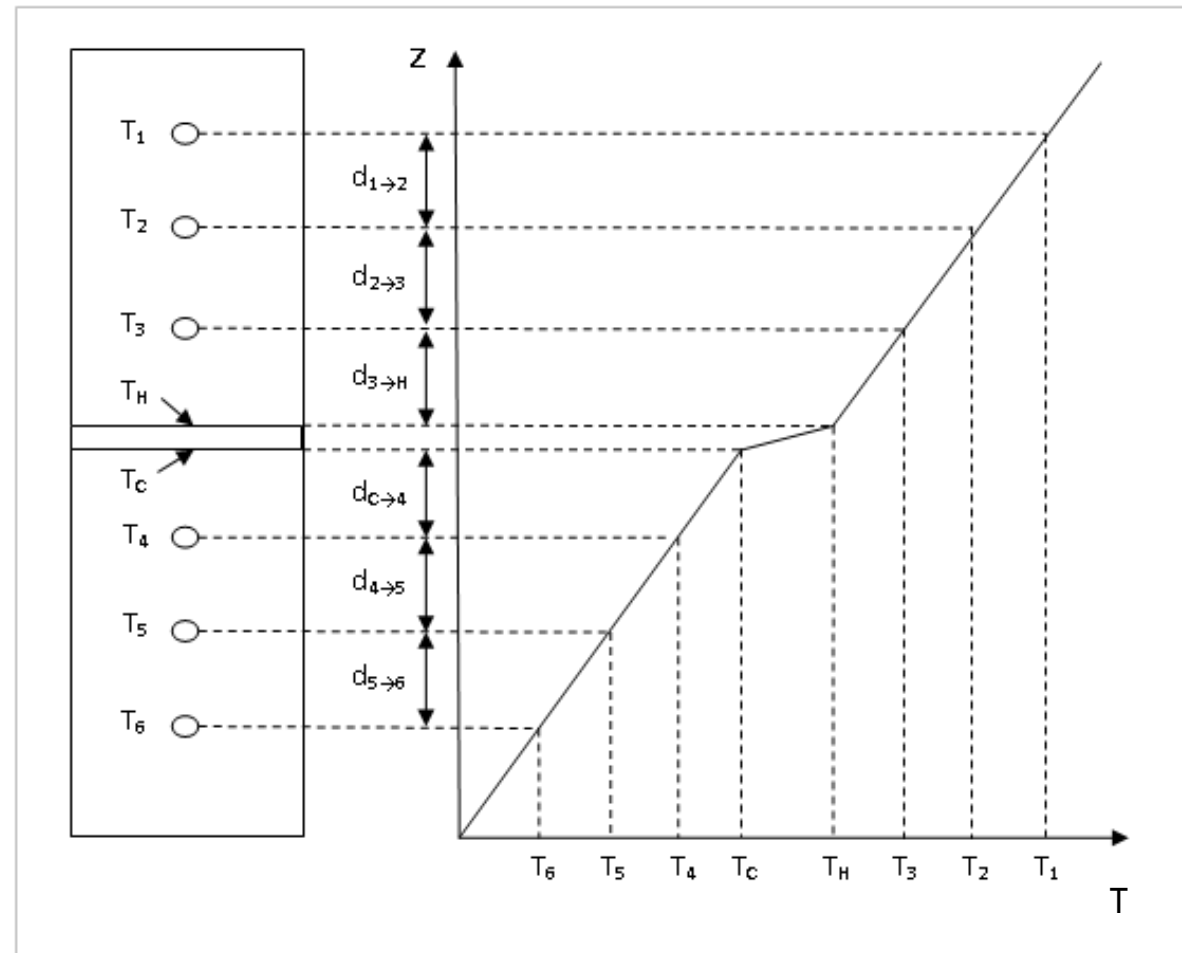


- An apparatus was designed to allow for steady state testing
- Steady state testing was based on the ASTM standard includes a guard heater, insulating sheath six RTD temperature sensors.
- The goal of the steady state test is to setup a one dimensional heat flow through the TIM sample



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$$\theta = QA^{-1}(T_H - T_C)^{-1}$$

$$\Delta T_{H \rightarrow C} = \Delta T_{3 \rightarrow 4} - d_{3 \rightarrow H} \left( \frac{dT}{dz} \right)_{hot} - d_{C \rightarrow 4} \left( \frac{dT}{dz} \right)_{cold}$$

$$\left( \frac{dT}{dz} \right)_{hot} = \frac{\Delta T_{1 \rightarrow 3}}{d_{1 \rightarrow 3}} \quad \left( \frac{dT}{dz} \right)_{cold} = \frac{\Delta T_{4 \rightarrow 5}}{d_{4 \rightarrow 5}}$$

$$Q = kA \left[ \frac{\left( \frac{dT}{dz} \right)_{hot} + \left( \frac{dT}{dz} \right)_{cold}}{2} \right]$$

$$\theta = \left[ \frac{k}{2} \left( \left( \frac{dT}{dz} \right)_{hot} + \left( \frac{dT}{dz} \right)_{cold} \right) \right] \left[ \Delta T_{3 \rightarrow 4} - d_{3 \rightarrow H} \left( \frac{dT}{dz} \right)_{hot} - d_{C \rightarrow 4} \left( \frac{dT}{dz} \right)_{cold} \right]^{-1}$$

$\theta$  = Thermal Conductance  
 $Q$  = Heat Flow  
 $k$  = Thermal conductivity of the meter bar  
 $A$  = Cross sectional area of the meter bar





# METHODOLOGY

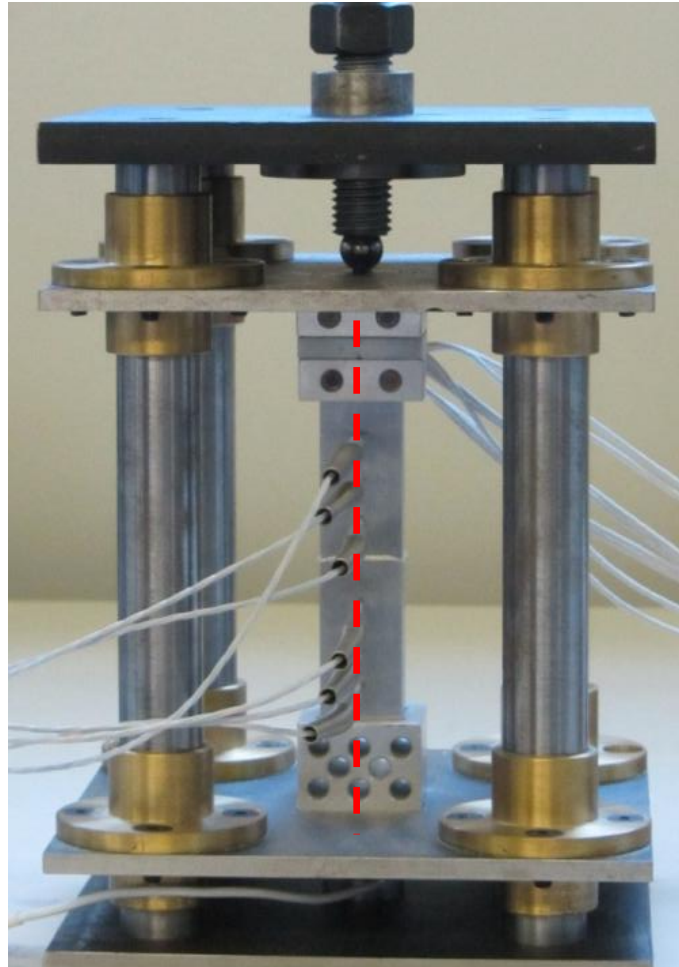
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# COMSOL MODEL

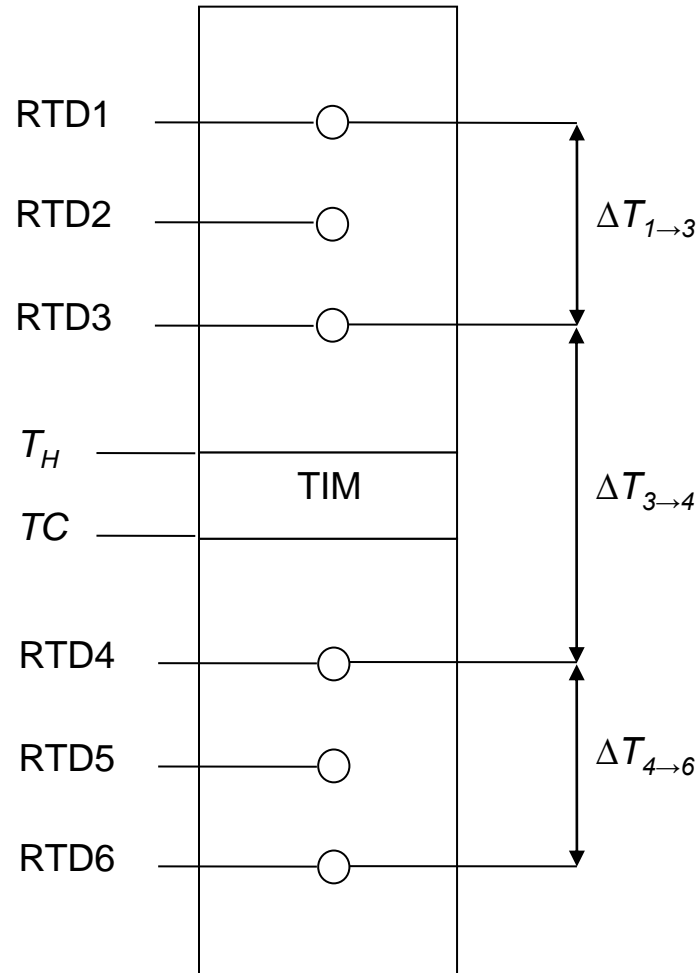
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<b>Material</b>	<b>Density (kg/m<sup>3</sup>)</b>	<b>Thermal Conductivity (W/mK)</b>	<b>Specific Heat (J/kgK)</b>
<b>Al 6061 T6</b>	2700	167	900
<b>Superwool 607</b>	335	0.06	0.243
<b>Macor</b>	2520	1.46	790
<b>Air</b>	COMSOL Materials Database		

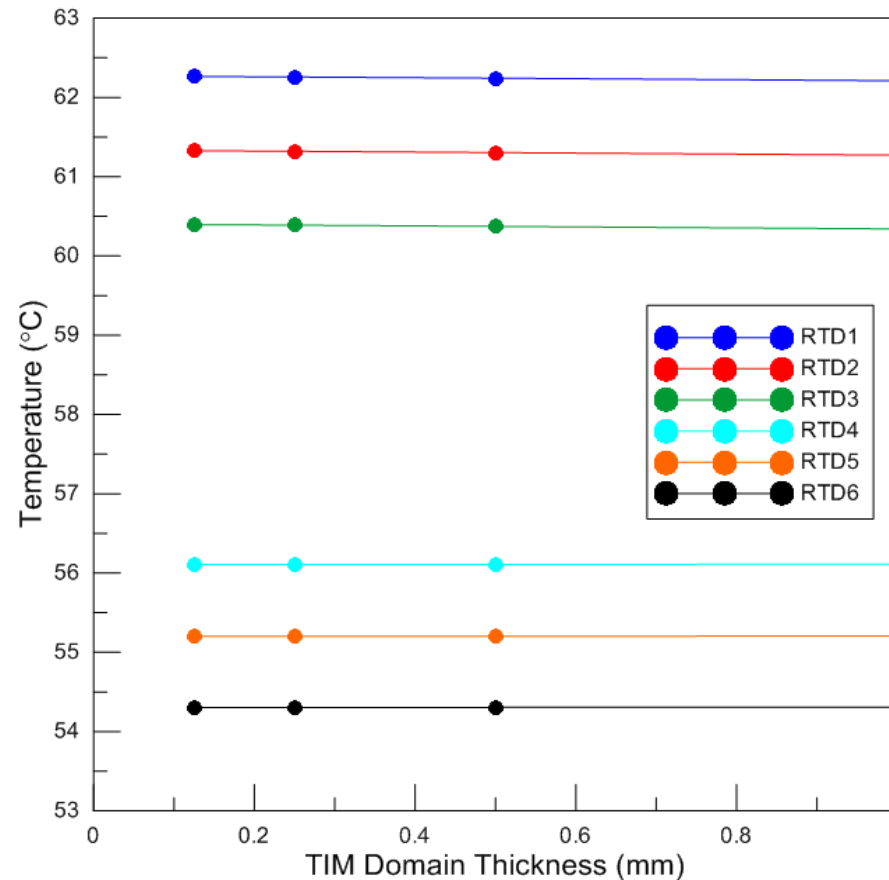
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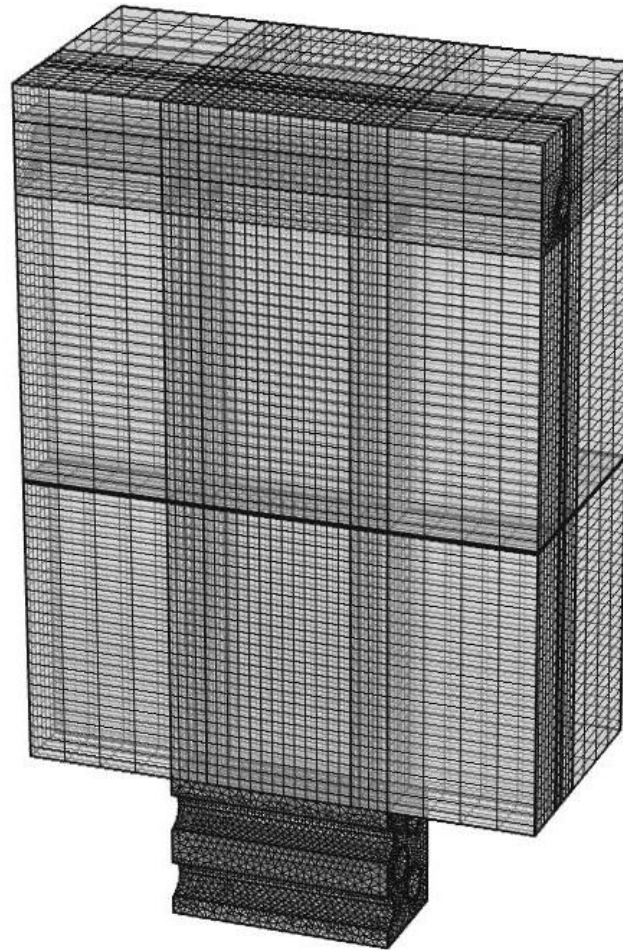
$$K_{TIMdomain} = d_{TIMdomain} \theta$$





# MESH

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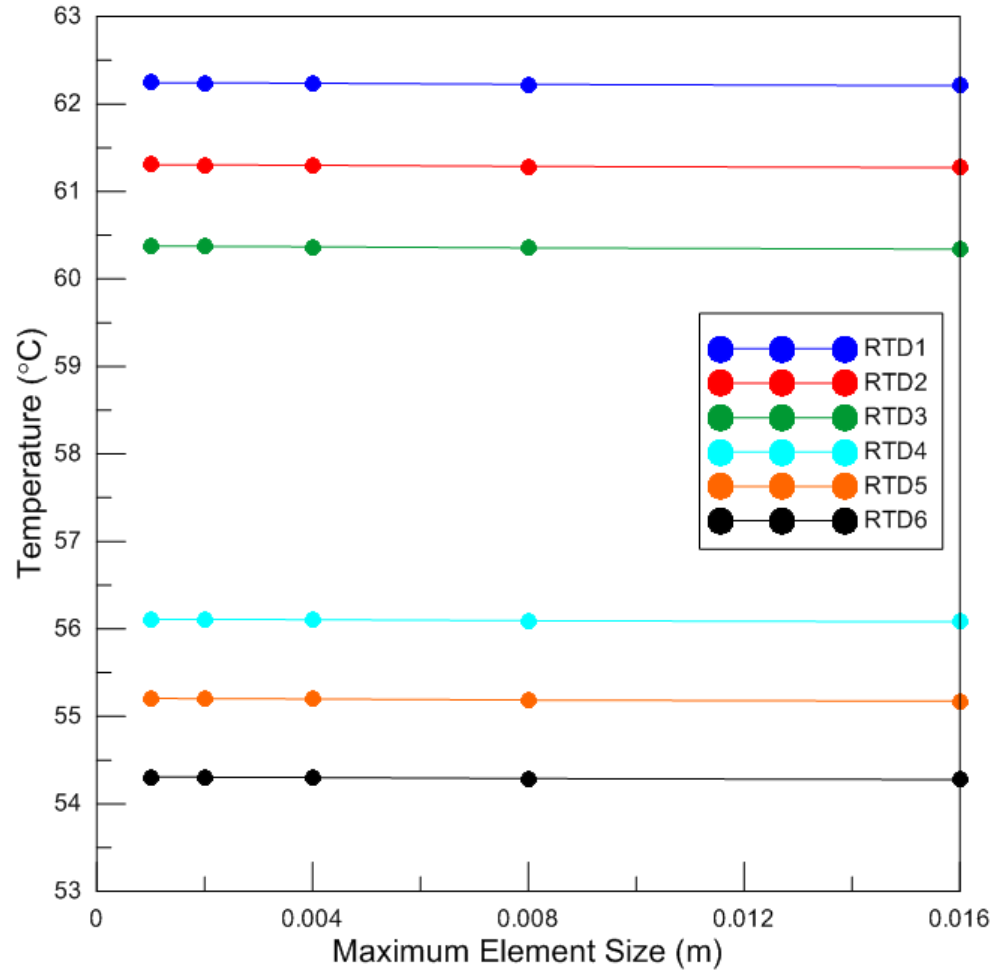
- Hex elements through most of the model, tetrahedral elements in the heat exchanger
- Maximum Element Size: 0.002 m
- 4 elements through the insulation layer: 0.0064 m





# MESH

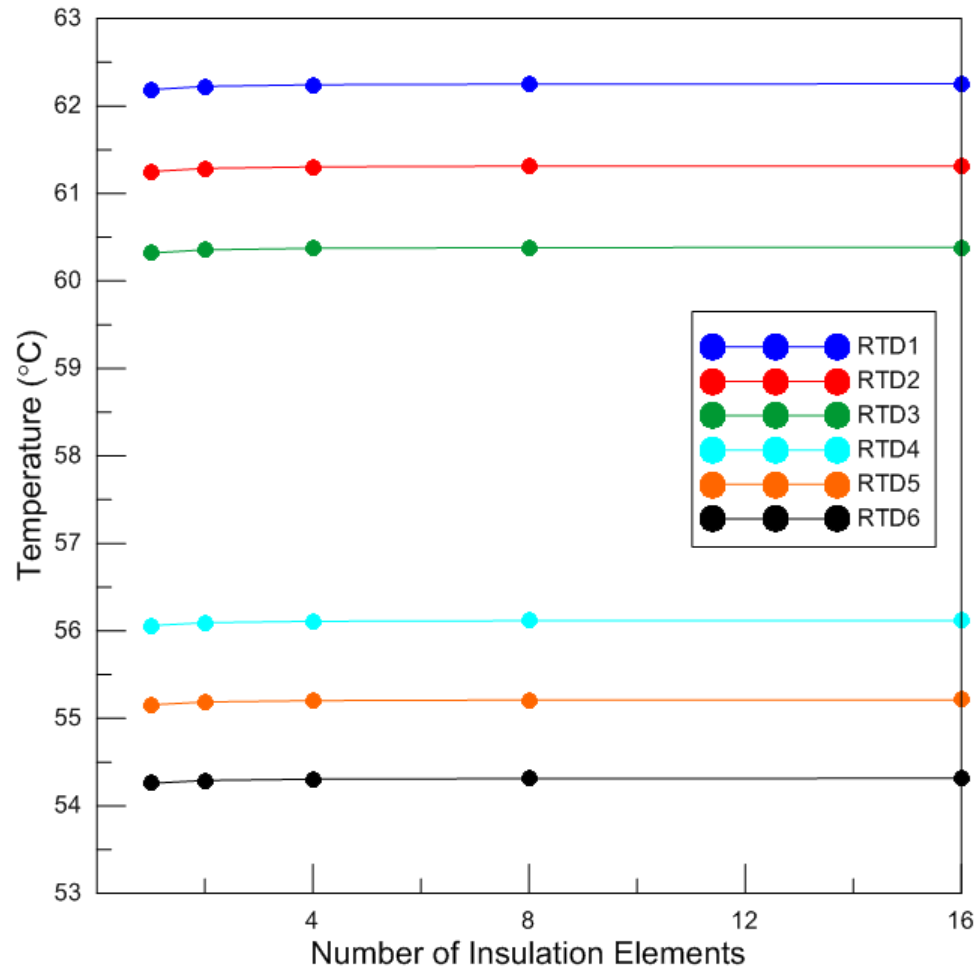
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# RESULTS

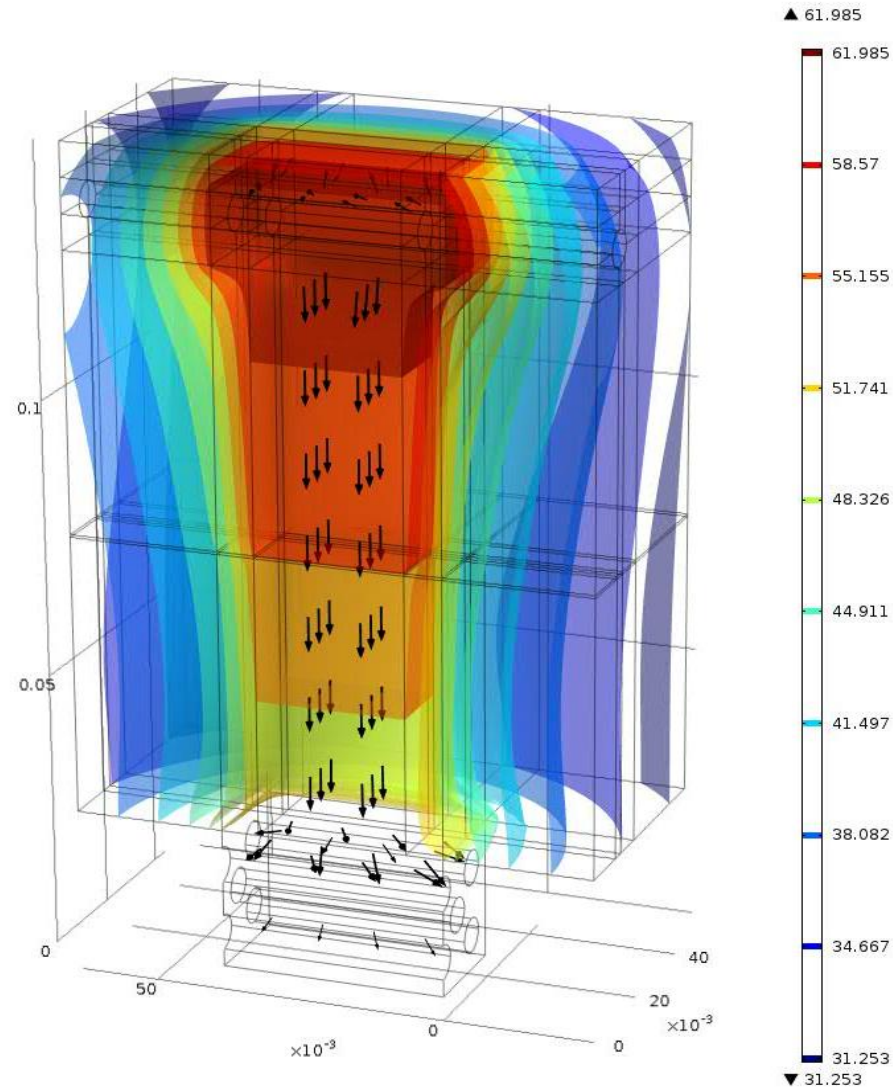
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- To do an initial test of the model the simplest experimental dataset was chosen: No TIM at 0.50 Mpa (73 psi)
  - This is a well understood case with few heat losses. Model is expected to match the one dimensional case well.

$h_{lateralheatloss}$	2.0 W/m <sup>2</sup> K
$h_{heatsink}$	36.1 W/m <sup>2</sup> K
$q_{topheatloss}$	1.1 W
$\theta$	?



# RESULTS

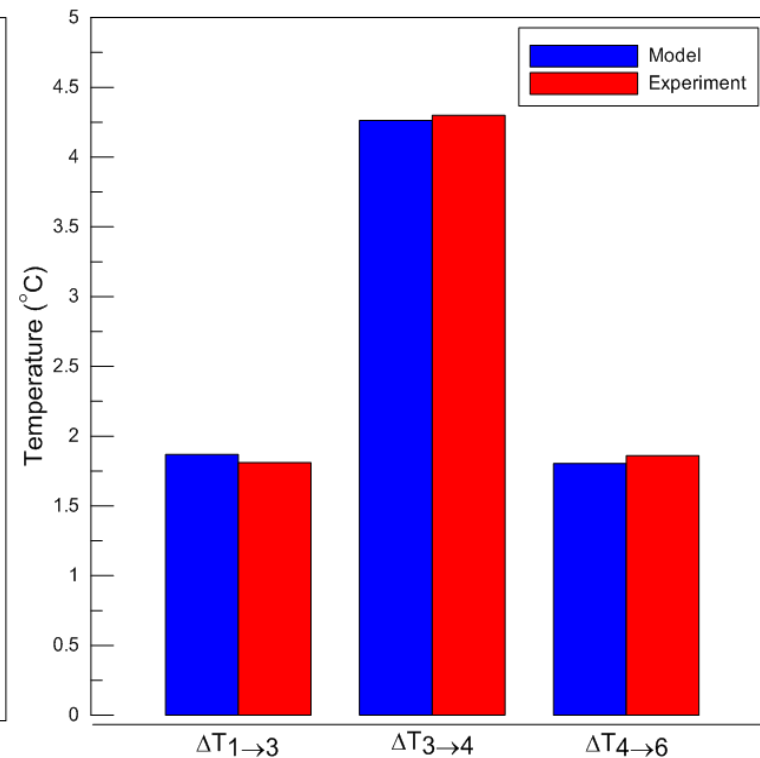
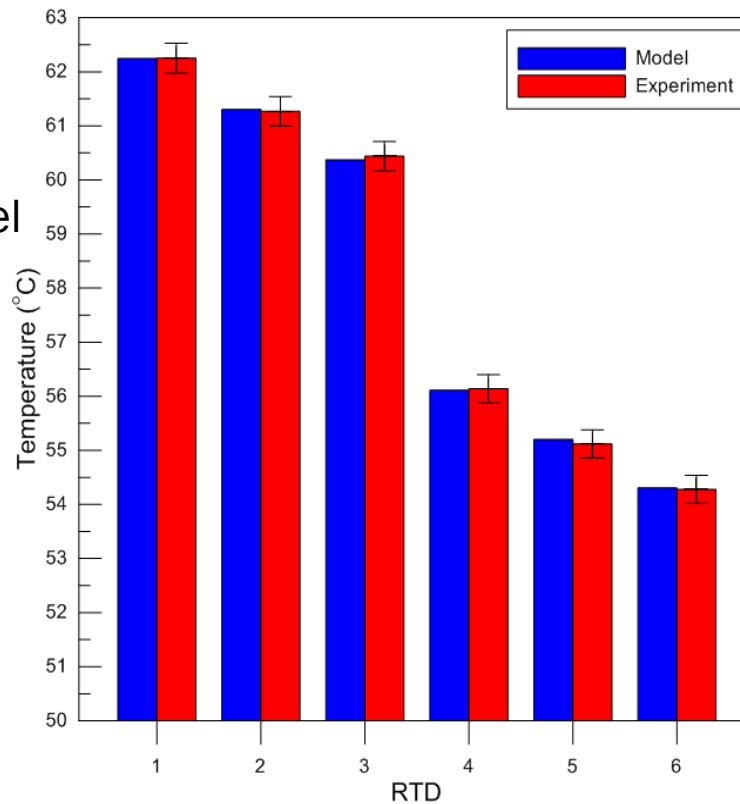
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$$\theta_{model} = 0.5 \text{ W/cm}^2\text{K} \quad \theta_{exp} = 0.49 \text{ W/cm}^2\text{K}$$



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- Initial comparisons with experimental data indicate that the FEA simulation works well.
  - Further comparing the model to more data sets, especially higher temperature tests where heat losses will be more significant, is the next step.
  - A sensitivity analysis on the FEA model would also be useful.



# REFERENCES

1. J. P. Gwinn, R. L Webb, Performance and testing of thermal interface materials. Microelectronics Journal, 34, 215-222, (2003)