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The Transient Modeling of Single-Bubble Nucleate Boiling in a Sub-Cooled Liquid Using an ALE Moving Mesh

> Christopher J. Forster Marc K. Smith

Georgia Institute of Technology Woodruff School of Mechanical Engineering

### Motivation

- Power electronics cooling using pool boiling heat exchangers.
- Models are being developed for pool boiling heat transfer with micro-channels in the presence of an acoustic field.
  - Increase critical heat flux (CHF) by delaying transition to film boiling.



 $\mu$ -channels  $\rightarrow$  350 W/cm<sup>2</sup>  $\mu$ -channels  $\rightarrow$  450 W/cm<sup>2</sup>



Photos courtesy of Thomas Boziuk and Ari Glezer Georgia Institute of Technology - Atlanta, GA

## **Previous Work**



### Present Work

- Two boiling models
   ALE single-bubble boiling
  - Level-set nucleate boiling





# **ALE Boundary Conditions**



### Normal-stress boundary condition

$$\left( \underline{\underline{\sigma}}_{\underline{l}} - \underline{\underline{\sigma}}_{\underline{g}} \right) \hat{n} = \sigma \kappa \hat{n} + P_{recoil}$$

$$\underline{\underline{\sigma}}_{g,l} = \left[ -P \underline{\underline{I}} + \eta \left( \nabla \underline{\underline{u}} + \left( \nabla \underline{\underline{u}} \right)^T \right) \right]_{g,l} \qquad \kappa = \nabla_{\!\! S} \cdot \hat{n}$$

#### Interface temperatures

 $T_l = T_v = T_{sat}$ 

#### **Vaporization**

 $\overline{q''_{vaporization}} = k_l \nabla T_l \cdot \widehat{\boldsymbol{n}}_l + k_v \nabla T_v \cdot \widehat{\boldsymbol{n}}_v$ 

#### Interface velocities

$$v_{n,l} = -\frac{q''vaporization}{\rho_l(h_v - h_l)} \qquad v_{n,v} = -\frac{q''vaporization}{\rho_v(h_v - h_l)}$$
$$(\underline{u} - \underline{u} \cdot \hat{n})_l - (\underline{u} - \underline{u} \cdot \hat{n})_v = 0$$
$$(\underline{u}_v \cdot \hat{n}_v - \underline{u}_l \cdot \hat{n}_l) + v_{n,l} + v_{n,v} = 0$$
$$u_{n,mesh} = \underline{u}_l \cdot \hat{n}_l + v_{n,l}$$

# Level-Set Boundary Conditions

**Temperature Recovery Method** 

 $\dot{m} = C\rho_l \left(\frac{T - T_{sat}}{T_{sat}}\right)$ Modified Continuity Equation  $\nabla \cdot \underline{u} = \delta \left(\frac{1}{\rho_v} - \frac{1}{\rho_l}\right) \dot{m} \hat{n}$ Interface Tangential Stress  $\hat{n} \cdot \left[\mu_l \left(\nabla \underline{u} + \nabla \underline{u}^T\right)_l - \mu_v \left(\nabla \underline{u} + \nabla \underline{u}^T\right)_v\right] \times \hat{n} = 0$ Interface Normal Stress  $-p_l + p_v + \hat{n} \cdot \left[\mu_l \left(\nabla \underline{u} + \nabla \underline{u}^T\right)_l - \mu_v \left(\nabla \underline{u} + \nabla \underline{u}^T\right)_v\right] \cdot \hat{n}$   $= \sigma \kappa - \left(\frac{1}{\rho_v} - \frac{1}{\rho_l}\right) \dot{m}^2$ 

Heat Source Term

 $\rho_f c_f \left( \frac{\partial \underline{\boldsymbol{u}}_f}{\partial t} + \underline{\boldsymbol{u}}_f \cdot \nabla T_f \right) = \nabla \cdot k_f (\nabla T)_f - \delta \dot{m} h_{lv}$ 



Modified Level–Set Equation  $\frac{\partial \phi}{\partial t} + \underline{U} \cdot \nabla \phi = 0$   $\underline{U} = \underline{u}_f + \frac{\dot{m}}{\rho_f} \hat{n}$ 

# **ALE Results**



### Slip Contact Line

Pinned Contact Line

### Level-Set Results



1/8<sup>th</sup> symmetry

2D Model

## Level-Set Results



1/8<sup>th</sup> symmetry



2D Model

# Summary

ALE model is good for modeling dynamics of a single bubble in greater detail.

Level-set offers the ability to model more complicated bubble interactions at the cost of interface detail.

# Future Work



### Combine benefits of ALE and level-set

### Boiling in micro-channels

- Effects of channel spacing, width, and depth
- Effects of contact angle
  - Material selection
  - Coatings

Determine fundamental mechanisms that allow the micro-channels to increase the critical heat flux

Add effects of acoustics

# Questions?

# Level-Set Reinitialization Error

