

Supercritical CO₂ leakage Modeling for Well Integrity in Geological Storage Project

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Houdu E., Meyer V., Poupard O. Oxand S.A., France

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✓ Context

Geological storage project

> OXAND's activities: Well Integrity Risk Analysis

✓ Modelling

Governing equations

> Porous media flow, biphasic system

✓ Results



Confirmation of global warming
 Kyoto agreement

 ✓ CO₂ market
 ■ legal framework, taxes



✓ EOR

Enhanced Oil Recovery

Growing interest for CO₂ geological storage as a feasible and relevant solution



CO₂ Injection and long-term geological storage in:

- Hydrocarbon reservoirs
- Saline aquifers
- Coal-bed



























✓ Biphasic flow model

- Water + Supercritical CO₂
- Incompressible phases
 - Fluids properties at p, T bottom injection reservoir

✓ Well modelling

Well is assumed as a concentric system
>Cylindrical coordinates





Computation stage

✓ Initial condition:

- Initial equilibrium
 Depletion period
- Injection

✓ Boundary condition

- Aquifer connection
 water
- Bottom reservoir connection
 > CO₂
- Surface connection
 - > atmosphere, water







✓ Wetting phase:

$$\delta_{s} \frac{\partial S_{w}}{\partial t} + \nabla \cdot \left[-\frac{k \cdot k_{r,w}}{\eta_{w}} \nabla (p_{w} + \rho_{w}gH) \right] = 0 \quad (1)$$

✓ Non-wetting phase:

$$\delta_{s} \frac{\partial S_{nw}}{\partial t} + \nabla \cdot \left[-\frac{k \cdot k_{r,nw}}{\eta_{nw}} \nabla (p_{nw} + \rho_{nw}gH) \right] = 0 \quad (2)$$



✓ Wetting phase:

$$C_{p,w} \frac{\partial (p_{nw} - p_w)}{\partial t} + \nabla \cdot \left[-\frac{k \cdot k_{r,w}}{\eta_w} \nabla (p_w + \rho_w gH) \right] = 0 \quad \textbf{(3)}$$

✓ Non-wetting phase:

$$C_{p,nw} \frac{\partial (p_{nw} - p_w)}{\partial t} + \nabla \cdot \left[-\frac{k \cdot k_{r,nw}}{\eta_{nw}} \nabla (p_{nw} + \rho_{nw} gH) \right] = 0 \quad \textbf{(4)}$$



✓ **Specific capacity** $C_{p,w} = -C_{p,nw} = \frac{\delta_s \partial S_w}{\partial p_c}$

 Relationship between effective water saturation and specific capacity

$$C_{p,w} = \frac{\alpha m}{1-m} \phi \left(1 - S_{r,w}\right) \Theta^{\frac{1}{m}} \left(1 - \Theta^{\frac{1}{m}}\right)^{m}$$



✓ Capillary pressure

$$p_c = p_{nw} - p_w$$

✓ Relationship to close biphasic flow model (Van Genuchten): $\left(1 + \left(\frac{p_c}{p_{ec}}\right)^N\right)^M = \frac{1}{\Theta}$ (7)

the effective saturation of wetting phase

$$\Theta = \frac{S_w - S_{rw}}{1 - S_{rw}}$$

■ the capillary pressure p_c

the capillary pressure head p_{ec}



			and the second





No CO₂ leakage with aquifer connection



No CO₂ leakage with aquifer connection



No possible CO₂ radial flow in the rat hole

Numerical difficulties

Space distortion

- Radial size scale: <1 m</p>
- Axial size scale: 1000 m

✓ Permeability

- Well cavity (50 D)
- Caprock (0.001 mD)
- Bad cement sheath (10 mD)

→ Large ranges of values for parameters describing the well induce numerical difficulties

✓ Capillary pressure head

- Need values > 0,1 bar to converge
- → Due to Van Genuchten model



- Numerical simulations have highlighted the competition between the gas flow and the liquid flow in a specific area of a well
- The rat-hole zone constitutes a key element to consider in the long term integrity performance of a well
- An improvement of the knowledge of the flows in this specific area within the well will be a support in assessing the Performance and the Risks from a well integrity perspective



✓ Robustness analysis to be performed

- To quantify the CO2 leakage in the case of no aquifer protection
- Improvements in the modeling to take into account the significant differences between some parameters values for two linked elements
- This study will have to be coupled to a macroscopic CO2 leakage modelling within well system.
 - Essential into a quantitative well integrity risk analysis for CO2 storage projects